# **EEE 3571 Electronic Engineering I**

# Lecture 8: Operational Amplifiers-Inverting Ckts



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# References

Our main reference text books in this course are

- [1] Neil S., Electronics: A Systems Approach, 4th edition, 2009, Pearson Education Limited, ISBN 978-0-273-71918-2.
- [2] Boylestad R. L., Nashelsky L., Electronic Devices and Circuit Theory, 11<sup>th</sup> Ed, 2013, Prentice-Hall, ISBN 978-0-13-262226-4.
- [3] Smith R. J., Dorf R. C., Circuits Devices and Systems, 5<sup>th</sup> Ed., 2004, John Wiley, ISBN ISBN 9971-51-172-X.

However, feel free to use pretty much any additional text which you might find relevant to our course.

# **Learning Objectives**

At the end of the lecture 10 on Op-Amps, you ought to:

- 1) Learn how these versatile amplifiers work and know how we can use them in practical circuits
- 2) Represent an amplifier by a simple circuit model and use the model to explain the features and behavior of an op amp and to analyze or design basic op-amp circuits for a variety of linear applications.
- 3) Learn about constant gain, summing, and buffering amplifiers.
- 4) Understand how an active filter network works.
- 5) Analyze or design useful circuits that take advantage of the nonlinear operating regions of the op amp, and understand some of the practical considerations in designing op-amp circuits.
- 6) Describe different types of controlled sources.
- 7) Arrange op amps to form an analog computer that can solve differential equations.

# **8.1 Introduction**

- ☐ The name operational amplifiers was first applied to amplifiers employed in analog computers to perform mathematical operations such as summing and integration.
- □ With sophisticated integrated-circuit (IC) amplifiers available for less than a dollar, the design of signal processing equipment has been radically altered.
- □ For linear or analog systems, the IC op amp plays the same basic building block role as do the IC logic and memory elements in digital systems.
- Combinations of op amps and digital devices are widely used in instrumentation and control.

# 8.2 Operational Amplifier (Op Amp)

Recall that a multistage amplifier is a complex circuit that combines basic designs (CB, CE, CC, Differential, Darlington, Current Mirror) to achieve optimum performance. It typically has three sections:



- (1) **Input Stage** This has one purpose: To provide the multi-stage amplifier with high input impedance e.g. differential amplifier.
- (2) Gain Stages This section consists of one or more amplifiers (stages) with high open-circuit voltage gain (e.g. common emitter). This stage provides the required voltage gain.
- (3) **Output Stage** This one's purpose: To provide the multi-stage amplifier with a low output impedance. This stage is commonly Common Collector (Emitter follower).





# **Components of 741 Operational Amplifier above**

- An Q1, Q2: Differential Amplifier (High input impedance, High voltage gain)
- □ Q3, Q4: Each forms cascode pair with Q1 and Q2 respectively (high frequency)
- Q8,Q9: Current Mirror for further reduction of Common Mode (CM) gain.
- Q10,Q11: Current Mirror for reference voltage from negative rail. They provide the slight base current needed by Q3 and Q4. Q10 has 5K resistor to limit current to almost zero.
- Q12,Q13: Current Mirror to act as active load to the Class A amplifier (Q15,Q19).
- Q14,Q20: Push Pull pair(Class AB). This is emitter follower and thus provides low output impedance and being a Class AB provides high current driving capability.
- □ Q16: Level shifting stage. This provides the Push-Pull pair with pre-biasing.
- □ Q17: Current limiting in Push-Pull's Q14.
- □ Offset Null (Pins 1 & 5): Zero out the output offset.

# **Operational Amplifier (Op Amp)**

### **Ideal Operational Amplifiers**

- An op amp is a direct-coupled, high-gain voltage amplifier designed to amplify signals over a wide frequency range. Typically, it has two input terminals and one output terminal and a gain of at least  $10^5$ , and it is represented by the symbol in Fig. 3b.
- □ It is basically a differential amplifier responding to the difference in the voltages applied to the positive and negative input terminals. (Single-input op amps correspond to the special case where the +ve input is grounded.)
- □ Normally we use an op amp with external feedback networks that determine the function performed.

□ The characteristics of an ideal op amp are as follows:

Voltage gain  $A = \infty$ Input impedance  $Z_i = \infty$ Output voltage  $v_o = 0$  when  $v_n = v_p$ Output impedance  $Z_o = 0$ Bandwidth  $BW = \infty$ Output impedance  $Z_o = 0$ 

# **Operational Amplifier (Op Amp)**



Fig. 3: Operational amplifier diagram, symbol, and pinout.

- Much as the aforesaid specifications are extreme, commercial units approach the ideal so closely that we can design many practical circuits assuming that these characteristics are available.
- One practical limitation that cannot be ignored is that, for linear operation, the output voltage  $v_o$  cannot exceed  $\pm V_{CC}$ .

- Usually, impedances  $Z_i$  and  $Z_o$  can be considered to be pure resistances  $R_i$  and  $R_o$  as shown in the model of Fig. 4*a*.
- □ The input signal is applied to the negative terminal and the positive terminal is grounded as depicted in the amplifier circuit of Fig. 4*b*.
- □ The input voltage  $v_1$  is applied in series with the resistance  $R_1$ , and the output voltage  $v_o$  is fed back through resistance  $R_F$ .



Fig. 4: The basic inverting amplifier circuit.

- □ Since the signal voltage is inverted, the feedback current is of opposite sign and  $i_F$  tends to cancel the input current  $i_1$ , leaving only a very small difference  $i_i$ .
- Another interpretation is that part of  $v_o$  fed back tends to cancel the effect of ,  $v_1$  leaving only a very small  $v_i$ ; we say that "the gain A drives  $v_i$  to zero."
- For an ideal op amp as in Fig. 4 *b*, closely approximated by a commercial unit,  $v_i = 0$  and  $i_i = 0$ ; therefore, the sum of the currents into node *a* is

$$i_1 + i_F = \frac{v_1}{R_1} + \frac{v_o}{R_F} = 0$$
 [1]

and the gain of the inverting amplifier circuit is

$$\frac{V_o}{V_1} = A_F = -\frac{R_F}{R_1}$$
 [2]



#### **Exercise 1**

 $\Box$  In the circuit of Fig. 4,  $R_i = 1 \text{ M}\Omega$ ,  $R_o \cong 0$ ,  $A = 2.5 \times 10^5$ ,  $R_1 = 10 \text{ K}\Omega$ , and

 $R_F = 1 \text{ M}\Omega$ . For  $v_o = -5 \text{ V}$ , calculate  $v_a = v_i$ ,  $v_1$ ,  $i_i$ , and  $i_1 = -i_F$ . In an ideal op amp,  $v_i/v_1 \ll 1$  and  $i_i/i_1 \ll 1$ ; on that basis, can this op amp be considered ideal?

#### [Solution]

$$v_a = v_i = 0.02 \text{ mV}, v_1 = 50 \text{ mV}, i_i = 0.00002 \ \mu\text{A}, i_1 = -i_F = 5 \ \mu\text{A}; \text{ yes.}$$

### **Low-pass Filter**

- A passive filter is frequency-selective network consisting of passive resistors, inductors, and capacitors. On the other hand, an active filter is one that incorporates amplifiers.
- □ They avoid the use of bulky and expensive inductors and have other advantages. Op amps with appropriate properties are used in active filters.





- Consider Fig. 5*a* as a simple example. It is a form of the general inverting amplifier circuit with impedance elements  $\mathbf{Z}_F(R \| C)$  and  $\mathbf{Z}_1(R_1)$  in the feedback network.
- $\Box$  Here  $V_1$  is a sinusoidal signal of variable frequency or a combination of signals of various frequencies. The voltage gain ( a function of frequency here)
  - is

$$\mathbf{A}_{F} = \frac{\mathbf{V}_{o}}{\mathbf{V}_{1}} = -\frac{\mathbf{Z}_{F}}{\mathbf{Z}_{1}} = -\frac{1/\left[\left(1/R\right) + j\omega C\right]}{R_{1}} = -\frac{R/R_{1}}{1 + j\omega RC}$$
[3]

The cutoff or half-power frequency is defined by  $\omega_{co}RC = 1$ , or



[4]

- □ The voltage gain decreases rapidly above  $\omega_{co}$  and this serves as a low-pass filter. The curve of Fig. 5b, drawn for  $R/R_1 = 100$ , does not exhibit a sharp cutoff.
- More complicated circuits designed by more sophisticated methods and using several op amps can provide sharp high-, low-, or band-pass filtering.
- □ In designing active filters for high-frequency applications, the frequency response of the op amp itself must be taken into account.
- □ Here we will assume that the range of frequencies passed is within the frequency response of the chosen op amp.



# [Example 8.1] Inverting Circuit Apps

□ A two-stage cascade amplifier circuit uses two of the low-pass filters of Fig. 5*a* in tandem. Thus, the output of the first stage is the input to the second stage. Find the overall gain  $\mathbf{A}_F = \mathbf{V}_o / \mathbf{V}_F$ . Also determine the gain well below and well above the cutoff frequency.

**[Solution]** When two ideal linear amplifiers are connected in tandem, the overall gain is the product of the voltage gains of the two stages, or

Therefore,  

$$\mathbf{A}_{F} = \frac{\mathbf{V}_{o}}{\mathbf{V}_{1}} = \frac{\mathbf{V}_{o}}{\mathbf{V}_{2}} \cdot \frac{\mathbf{V}_{2}}{\mathbf{V}_{1}}$$

$$\mathbf{A}_{F} = \left(-\frac{R}{R_{1}\left(1+j\omega RC\right)}\right) \left(-\frac{R}{R_{1}\left(1+j\omega RC\right)}\right)$$

$$= \left(\frac{R}{R_{1}}\right)^{2} \left(\frac{1}{1+j\omega RC}\right)^{2}$$

At 
$$\omega = \omega_{co}$$
 the magnitude of the gain is,
$$A_{F} = \left(\frac{R}{R_{I}}\right)^{2} \frac{1}{1 + \omega_{co}^{2} (RC)^{2}} = \left(\frac{R}{R_{I}}\right)^{2} \frac{1}{1 + (1/RC)^{2} (RC)^{2}}$$

$$= \frac{1}{2} \left(\frac{R}{R_{I}}\right)^{2} = A_{co}$$
For frequencies well below  $\omega_{co}$ ,  $\omega RC <<1$  and the gain is
$$A_{Io} \approx \left(\frac{R}{R_{I}}\right)^{2} \left(\frac{1}{1+0}\right)^{2} = \left(\frac{R}{R_{I}}\right)^{2} = 2A_{co}$$
For frequencies well above  $\omega_{co}$ ,  $\omega RC >>1$  and the gain
$$A_{Io} \approx \left(\frac{R}{R_{I}}\right)^{2} \left(\frac{1}{\omega RC}\right)^{2} = \frac{1}{\omega^{2}} \left(\frac{1}{R_{I}C}\right)^{2}$$
is inversely proportional to the square of the frequency.

#### **Exercise 2**

□ Consider a circuit similar to that of Fig. 5a with the capacitor *C* connected in series with the resistor *R* instead of in parallel. Derive an expression for the voltage gain as a function of frequency  $\omega$  and describe the characteristics of this circuit.

$$\mathbf{A}_{F} = -\left(\frac{1}{R_{1}}\right)\frac{1+j\omega RC}{j\omega C} = -\frac{R}{R_{1}}\left(1+\frac{1}{j\omega RC}\right)$$

□ The circuit is simply a high-pass filter.



### **Summing Circuit**

- If the circuit in Fig. 4 is modified to permit multiple inputs, the operational amplifier can perform addition.
- In Fig. 6, the input current is supplied by several voltages through separate resistances. In the practical case,  $v_i = 0$  and  $i_i = 0$  and the circuit model is as shown in Fig. 6b. The sum of the input currents is just equal and opposite to the feedback current, i.e., [5]

$$i = i_1 + i_2 + \dots + i_n = -i_F$$

 $v_0 = -\left[ v_1 (R_F/R_1) + v_2 (R_F/R_2) + \dots + v_n (R_F/R_n) \right]$ 

Let The second strain I and the second strain I and the second strain I and the second strain strain

$$\frac{v_1}{R_1} + \frac{v_2}{R_2} + \dots + \frac{v_n}{R_n} = -\frac{v_0}{R_F}$$

**Thus**,

The output is the weighted sum of the inputs. Note, that a signal can be subtracted using an inverting amplifier with  $R_F = R_1$ .

#### **Digital to Analog Converter**

- □ To translate a digital number to an analog signal, we need a digital-to-analog converter (DAC). A DAC is a device that converts a digital input number sequence into an equivalent analog signal.
- Most commonly, the digital input is a binary word and the analog output is a voltage or current. For example, the 4-bit number

$$1100 = 1 \times 2^3 + 1 \times 2^2 + 0 \times 2^1 + 0 \times 2^0 = 8 + 4 + 0 + 0 = 12D$$
 [7]

could be translated to an output signal amplitude of 12 V. The conversion involves a weighted sum corresponding to the output of the op amp summing circuit of Fig. 4.

#### **Exercise 3**

□ Design a digital-to-analog converter to convert the binary number stored in a 4bit register into decimal-equivalent voltage. Assume the register provides inputs at precisely 0 V and +4 V. Let  $R_F = 20 \text{ k}\Omega$ .



# [Solution]

 $R_1(MSB) = 10 \text{ k}\Omega, R_2 = 20 \text{ k}\Omega, R_3 = 40 \text{ k}\Omega, R_4(LSB) = 80 \text{ k}\Omega.$ 

- □ For accurate conversion, the inputs to a summing-circuit DAC would have to have precisely known voltages, a condition that is NOT required in digital systems.
- □ The various weighting resistances would also have to be precisely formed, a very difficult requirement in an IC 16-bit converter. In practice, the *R*-2*R* ladder of Fig. 7*a* is far superior.
- □ To predict the behavior of the *R*-2*R* DAC, we replace the ladder by its Thevenin equivalent. With all voltage sources removed, we note that the resistance to the left of node 4 is R + R = 2R.
- □ The equivalent resistance to the left of node 3 is

 $R + 2R \| 2R = 2R$ 





Fig. 7: The *R*-2*R* ladder op amp DAC.

which is the same for nodes 2 and 1.

■ By voltage division, the contribution of source  $v_1$  is  $v_1(2R/4R) = v_1/2$ . After redrawing the circuit, the contribution of source  $v_2$  is seen to be  $v_2(2R/4R)(2R/4R) = v_2/4$ . Thus, the complete Thevenin equivalent is

$$v_T = \frac{v_1}{2} + \frac{v_2}{4} + \frac{v_3}{8} + \frac{v_4}{16}$$
 and  $R_T = R$  [8]

□ As shown in Fig. 7*b*, for  $R_F = 16R$  the output voltage is

$$v_o = -(8v_1 + 4v_2 + 2v_3 + v_4)$$
[9]

- Therefore, this circuit provides the desired conversion using only two resistance values. Furthermore, only resistance ratios must be precise (easy to provide in ICs), and it turns out that the resistance "seen" by each binary source is the same (desirable for uniform behavior).
- □ The practical result is that high-precision DACs are available at low cost.

#### Current/Voltage Converters Self Study

An example of op amp versatility is in driving a low-resistance load (a coil, for instance) with a voltage source of high internal resistance.





Fig. 8: Voltage-current converter circuits.

A good constant-current source for a grounded load can be made from an op amp and an external transistor. In Fig. 8*a*, reference voltage  $V_1$  is obtained from a voltage divider.



Self Study

#### Self Study

# **Inverting Circuit Applications**

- □ Feedback drives  $V_i$  to zero so that  $V_E = V_1$ ; if  $V_E$  tends to fall below  $V_1$ , the forward bias on the base-emitter (*np*) junction decreases and emitter current  $I_E$  drops, bringing  $V_E$  back to  $V_1$ .
- In effect, a voltage  $V_s V_1 = V_s \cdot R_2 / (R_1 + R_2)$  establishes an emitter current in the *pnp* transistor and current

$$I_{L} = I_{C} \cong I_{E} = \frac{V_{S} \cdot R_{2} / (R_{1} + R_{2})}{R} = V_{S} \frac{R_{2}}{R(R_{1} + R_{2})}$$
[10]

is maintained in a changing load  $R_L$ . The voltage source  $V_S$  has been converted into a current source  $I_L$ .

The inverse function is performed by circuit of Fig. 6*b*. Here a given current  $I_s$  is introduced into the *-ve* terminal of the op amp, setting up an equal current in the feedback resistor  $R_F$ . Because the amplifier input voltage is practically zero, the output voltage is



#### Self Study

# **Inverting Circuit Applications**

$$V_o = -I_F R_F = -I_S R_F$$
[11]

- and the source current has been converted to voltage.
- □ The current-to-voltage converter is useful where a current is to be measured without introducing an undesired resistance  $R_{oF} \cong 0$  or where a current source, such as photocell, has a high shunt resistance.

# [Example 8.2] Inverting Circuit Applications



□ A photocell generates 0.2  $\mu$ A of current per  $\mu$ W of radiant power for a constant reverse-bias voltage. Design a circuit to measure radiant power with a voltmeter.

# [Solution]

Fig. 9: Photodiode light meter.

# [Example 8.2] Inverting Circuit Self Study Applications Cont'd

- The photocurrent  $I_D$  could be allowed to flow through a resistance to develop a measurable voltage, but this voltage would reduce the reverse bias and alter the photodiode characteristic.
- □ From the circuit in Fig. 9, since  $v_i \cong 0$ , there is no bias voltage change with a change in  $I_D$ .

If  $R_F = 5 k\Omega$  and the radiant power is 100  $\mu$ W, the voltmeter will read

 $V_M = I_D R_F = (100 \times 0.2) \times 10^{-6} \times 5 \times 10^3 = 100 \text{ mV}$ 

and the scale factor of the "light meter" is  $1 \,\mu W/mV$ .



**Fig. 10**: A direct-coupled differential amplifier.

### **Differential Amplifier**

- ❑ The direct-coupled differential amplifier shown in Fig. 10 is widely used in instrumentation.
- In the typical transducer, a physical variable such as a change in temperature or pressure is converted to an electrical signal that is then amplified to a useful level.
- The differential amplifier is advantageous because it discriminates against dc variations, drifts, and noise and responds only to significant changes.



- In Fig. 10, voltages  $v_1$  and  $v_2$  represent variables measured at two points in a complicated system, like the human body.
- We see that the measurements include a large common-mode voltage and a small differential voltage. The common-mode voltage has a dc component, perhaps due to drift of operating temperature, and a sinusoidal "hum" component picked up from power lines.
- □ The small differential voltage  $v_p v_n$  is the signal that we are interested in and wish to amplify.
- □ In the circuit of Fig. 10, assume an ideal op amp,  $v_i = 0$  and the potential at node x is equal to the voltage across  $R_3$ , or

$$v_{3} = \left(v_{cm} + v_{p}\right) \frac{R_{3}}{R_{2} + R_{3}} = v_{x}$$
[12]

 $\square$  Because  $i_i = 0$ , the currents  $i_1$  and  $i_F$  are equal, or

$$i_1 = \frac{v_{cm} + v_n - v_x}{R_1} = i_F = \frac{v_x - v_o}{R_F}$$
[13]

[15]

Combining Eqs. [12] and [13] yields

$$v_{o} = v_{cm} \left( \frac{R_{3}}{R_{2} + R_{3}} - \frac{R_{F}}{R_{1}} + \frac{R_{F}}{R_{1}} \cdot \frac{R_{3}}{R_{2} + R_{3}} \right) + v_{p} \left( \frac{R_{3}}{R_{2} + R_{3}} + \frac{R_{F}}{R_{1}} \cdot \frac{R_{3}}{R_{2} + R_{3}} \right) - v_{n} \left( \frac{R_{F}}{R_{1}} \right)$$
[14]

If we design the network so that  $R_F/R_1 = R_3/R_2$ , the coefficient of  $v_{cm}$  goes to zero, the common-mode signal is rejected, and the output is

$$v_o = -\frac{R_F}{R_1} \left( v_n - v_p \right)$$

□ The ability to reject the common-mode signal is a valuable feature of a DA.

#### **Exercise** 4

□ In a direct-coupled differential amplifier,  $R_1 = 10 \text{ k}\Omega$  and  $R_2 = 20 \text{ k}\Omega$ . Specify  $R_3$  and  $R_F$  for common-mode signal rejection and a differential amplifier gain of 50. If the inputs are  $v_1 = 5 + \sin 100t + 0.05 \sin 5000t$  V and  $v_2 = 5 + \sin 100t - 0.03 \sin 5000t$  V, predict the output voltage.

# [Solution]

 $R_3 = 1 \text{ M}\Omega, R_F = 0.5 \text{ M}\Omega, v_o = 4 \sin 5000t \text{ V}$ 

### **Analog Integrator ckt**

- □ So far, the input and feedback components have been resistors. If the feedback component used is a capacitor as shown in Fig 11a, the ckt is called an integrator. The virtual-ground equivalent ckt is shown in Fig 11b.
- □ Recall that the virtual ground entails the voltage at the junction of  $R_1$  and  $X_c$  to be ground, that is,  $v_i \approx 0$ , but not current goes into the ground at that point.





Fig. 11: Integrator circuit.

The capacitive impedance can be expressed as

$$X_C = \frac{1}{j\omega C} = \frac{1}{sC}$$
[16]

[17]

where  $s = j\omega$  is in *Laplace notation*. Thus, solving for  $V_o/V_1$  yields  $I_1 = \frac{V_1}{R_0} = -\frac{V_o}{1/sC} = -sCV_0$ 

□ It follows from Eq. [17] that,

$$\frac{V_o}{V_1} = -\frac{1}{sCR_1}$$
[18]

Eq. [18] can be rewritten in the time domain by its inverse Laplace transform as

$$v_o(t) = -\frac{1}{R_1 C} \int v_1(t) dt$$
[19]

[20]

- □ Eq. [19] shows that the output is the integral of the input, with an inversion and scaled multiplier of  $1/R_1C$ .
- □ It is worth noting that more than one input may be applied to an integrator, as shown in Fig. 12, with the resulting operation given by

$$v_{o}(t) = -\left[\frac{1}{R_{1}C}\int v_{1}(t) dt + \frac{1}{R_{2}C}\int v_{2}(t) dt + \frac{1}{R_{3}C}\int v_{3}(t) dt\right]$$



**Fig. 12**: Summing-Integrator circuit.

# **[Example 8.3] Inverting Circuit Applications**

□ Consider the ckt in Fig. 12, let the values of the input resistors and feedback capacitor be,  $R_1 = 200 \text{k}\Omega$ ,  $R_2 = 100 \text{k}\Omega$ ,  $R_3 = 1 \text{M}\Omega$ , and  $C = 1 \mu \text{F}$ . Find the output voltage when all inputs are unit step voltages, i.e., 1V.

# [Solution]

From Eq. [20] it follows that

# [Example 8.3] Inverting Circuit Applications Cont'd

### **Analog Differentiator ckt**

❑ A differentiator circuit is shown in Fig. 13. Much as it is not as useful as the integrator ckt we just looked at, the differentiator does provide a useful operation. The resulting relation for the circuit is

$$v_o(t) = -RC \frac{dv_1(t)}{dt}$$

[21]



Fig. 13: Differentiator circuit.

### **OP-Amp Specifications-DC Offset Parameters**

□ It is worth while to become familiar with some of the parameters used to define the operation of the op-amp. This is critical in practical applications.

### **Offset Currents and Voltages**

- □ Although the op-amp output should be 0V when the input is 0V, in actual operation there is an offset voltage at the output.
- □ For instance, if one connected 0V to both inputs and then measured 26mV (dc) at the output, this an unwanted voltage generated by the ckt and not the input.
- □ The manufacturer specifies an input offset voltage for the op-amp. The output offset voltage is then determined by input offset voltage and the gain of the amplifier, as connected by the user.
- The output offset voltage is affected by; an input offset voltage  $V_{IO}$  and an offset current due to the difference in currents resulting at the +ve and –ve inputs.



#### Input Offset Voltage

The manufacturer's specification sheet provides a value of  $V_{IO}$  for the opamp. To determine the effect of this input voltage on the output, consider the connection shown in Fig. 14. Using  $V_o = AV_i$ , we can write



 $V_o = V_{IO} \frac{1}{1 + A \left[ R_1 / \left( R_1 + R_f \right) \right]}$ [23]

[22]

From Eq. [23] we can write

$$V_o(\text{offset}) = V_{IO} \frac{R_1 + R_f}{R_1}$$

[24]

☐ From Eq. [24] shows how the output offset voltage results from a specified input offset voltage for a typical amplifier connection of the op-amp.



#### **Output Offset Voltage Due to Input Offset Current**

- An output offset voltage will also result due to any difference in dc bias currents at both inputs.
- □ Since the two input transistors are never exactly matched, each will operate at a slightly different current.
- Consider a typical op-amp connection in Fig. 16a, an output offset voltage can be determined as follows.



- Replacing the bias currents through the input resistors by the voltage drop that each develops as shown in Fig. 14b, we can determine the expression for the resulting output voltage.
- By superposition, we see that the output voltage due to the input bias current  $I_{IB}^+$  denoted by  $V_o^+$  is given by

$$V_o^+ = I_{IB}^+ R_C \left( 1 + \frac{R_f}{R_1} \right)$$
[25]

 $\Box$  whereas the output voltage due to only  $I_{IB}^-$ , denoted by  $V_o^-$ , is given by

$$V_o^- = I_{IB}^- R_1 \left( -\frac{R_f}{R_1} \right)$$
[26]

Thus, the total offset voltage is

$$V_o$$
 (offset due to  $I_{IB}^+$  and  $I_{IB}^-$ ) =  $I_{IB}^+ R_C \left(1 + \frac{R_f}{R_1}\right) - I_{IB}^- R_1 \left(\frac{R_f}{R_1}\right)$  [27]

Since the main consideration is the difference between the input bias currents rather than each value, we define the offset current  $I_{IO}$  by

$$I_{IO} = I_{IB}^{+} - I_{IB}^{-}$$
 [28]

□ Since the compensating resistance  $R_c$  is usually approximately equal to the value of  $R_1$ , using  $R_c = R_1$  in Eq. [27], we can write

$$V_{o} (\text{offset}) = I_{IB}^{+} (R_{1} + R_{f}) - I_{IB}^{-} R_{f}$$
  
=  $I_{IB}^{+} R_{f} - I_{IB}^{-} R_{f} = R_{f} (I_{IB}^{+} - I_{IB}^{-})$  [29]

**Resulting in** 

$$V_o$$
 (offset due to  $I_{IO}$ ) =  $I_{IO}R_f$  [30]

## [Example 8.5] Inverting Circuit Applications

Calculate the offset voltage of the ckt in Fig. 14 for the op-amp spec listing  $I_{IO} = 100 \text{ nA}$ .

[Solution]

Using Eq. [30], 
$$V_o = I_{IO}R_f = (100 \text{ nA})(150 \text{ k}\Omega) = 15 \text{ mV}$$

#### Total Offset Due to $V_{IO}$ and $I_{IO}$ .

The total offset voltage due to both factors covered above can be expressed as

 $|V_o(\text{offset})| = |V_o(\text{offset due to } V_{IO})| + |V_o(\text{offset due to } I_{IO})|$ 

[32]

The absolute magnitude is used to accommodate the fact that the offset polarity may be either positive or negative.

□ Input Bias Current,  $I_{IB}$ . A parameter related to  $I_{IO}$  and the separate input currents  $I_{IB}^+$  and  $I_{IB}^-$  is the average current defined as

$$I_{IB} = \frac{I_{IB}^+ + I_{IB}^-}{2}$$

□ One could determine the separate input bias currents using the specified  $I_{IO}$ and  $I_{IB}$ . It can be shown that for  $I_{IB}^+ > I_{IB}^-$ 

$$I_{IB}^{+} = I_{IB} + \frac{I_{IO}}{2}$$
 and  $I_{IB}^{-} = I_{IB} - \frac{I_{IO}}{2}$  [33]

# **End of Lecture 8**

# Thank you for your attention!