

EE321

ELECTROMECHANICS & ELECTRICAL MACHINES

UNIVERSITY EXAMINATIONS

NOVEMBER/DECEMBER 2011

MODEL SOLUTIONS

1.

(a)

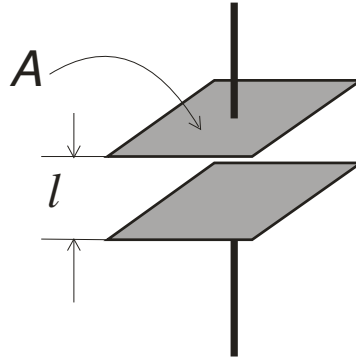
A = plate area

l = distance of separation

$$C = \frac{Q}{V}$$

$$= \frac{DA}{El}$$

$$C = \underline{\underline{\epsilon \frac{A}{l}}}$$



(b)

$l = 15 \text{ mm}$, $V = 20 \text{ kV}$, $\epsilon_r = 26$.

(c)

$l = 1 \text{ km}$, $V = 10 \text{ kV}$, $\epsilon_r = 4$, $f = 50 \text{ Hz}$, $d_l = 2r_l = 12 \text{ mm}$, $t = 4 \text{ mm}$.

$$(i) C = \frac{2\pi l \epsilon}{\ln \frac{r_2}{r_1}} = \frac{2\pi \times 1 \times 10^3 \times (4 \times 8.85 \times 10^{-12})}{\ln \left(\frac{6+4}{6} \right)} = 4.35 \times 10^{-7} = \underline{\underline{43.5 \text{ } \mu\text{F}}}$$

$$(ii) \hat{W} = \frac{1}{2} C \hat{V}^2 = \frac{1}{2} \times 4.35 \times 10^{-7} \times (1 \times 10^3)^2 = \underline{\underline{0.218 \text{ J}}}$$

$$(iii) |I| = V \omega C = 2\pi f V C = 2\pi \times 50 \times (1 \times 10^3) \times 4.35 \times 10^{-7} = \underline{\underline{0.137 \text{ A}}}$$

2.

(a)

$$\Lambda = \frac{\phi}{F} = \frac{BA}{Hl} = \mu \frac{A}{l}$$

$$S = \frac{1}{\Lambda} = \frac{l}{\mu A}$$

$$\text{Circuit: } v = L \frac{di}{dt} \text{ and Faraday's law; } v = N \frac{d\phi}{dt}$$

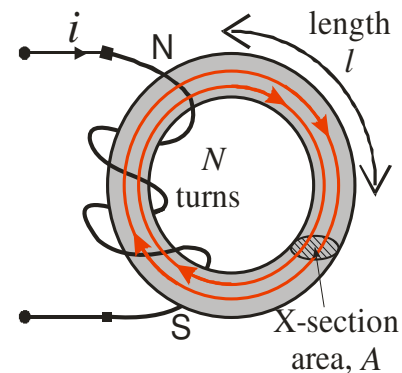
$$L \frac{di}{dt} = N \frac{d\phi}{dt}$$

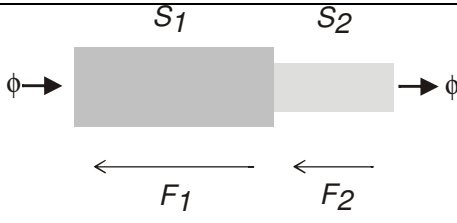
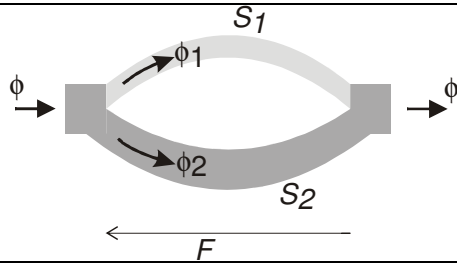
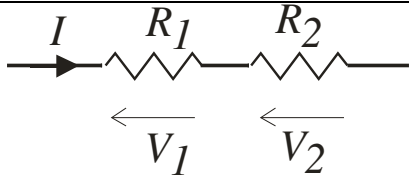
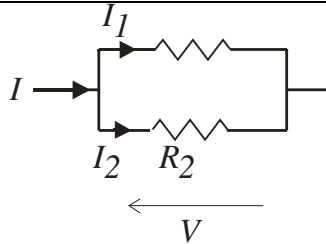
$$L = N \frac{d\phi}{di}$$

$$\text{Uniform case: } L = N \frac{\phi}{i} \text{ and } \phi = \frac{F}{S} = \frac{Ni}{S}$$

$$\therefore L = \underline{\underline{\frac{N^2}{S}}}$$

(b)



	Series combination	Parallel combination
Magnetic		
	$F = F_1 + F_2$ $\frac{F}{\phi} = \frac{F_1}{\phi} + \frac{F_2}{\phi}$ $S_{tot} = S_1 + S_2$	$\phi = \phi_1 + \phi_2$ $\frac{\phi}{F} = \frac{\phi_1}{F} + \frac{\phi_2}{F}$ $\frac{1}{S_{tot}} = \frac{1}{S_1} + \frac{1}{S_2}$
		
	$V = V_1 + V_2$ $\frac{V}{I} = \frac{V_1}{I} + \frac{V_2}{I}$ $R_{tot} = R_1 + R_2$	$I = I_1 + I_2$ $\frac{I}{V} = \frac{I_1}{V} + \frac{I_2}{V}$ $\frac{1}{R_{tot}} = \frac{1}{R_1} + \frac{1}{R_2}$

(c)

$$B = 1.2 \text{ T}, l_g = 1 \text{ mm}, l_{Fe} = 80 \text{ cm}, A = 20 \text{ cm}^2.$$

$$(i) S_g = \frac{l_g}{\mu A} = \frac{1 \times 10^{-3}}{4\pi \times 10^{-7} \times (20 \times 10^{-4})} = 397,887 \text{ A/Wb}$$

$$S_{Fe} = \frac{l_{Fe}}{\mu A} = \frac{80 \times 10^{-2}}{10^{-3} \times (20 \times 10^{-4})} = 400,000 \text{ A/Wb}$$

$$S_{tot} = 2 \times S_g + S_{Fe} = 2 \times 397887 + 400000 = 1,195,774 \text{ A/Wb}$$

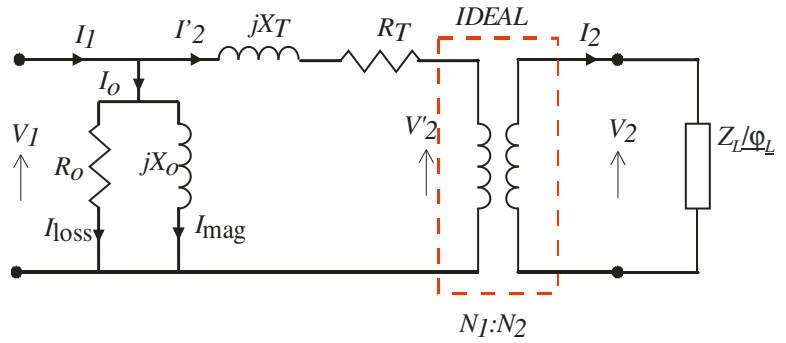
$$F = \phi S_{tot} = BAS_{tot} = 1.2 \times (20 \times 10^{-4}) \times 1195774 = 2869 \approx \underline{\underline{2870 \text{ A}}}$$

$$(ii) F = "PA" = \frac{1}{2} \frac{B^2}{\mu} (2A) = \frac{1}{2} \times \frac{1.2^2 \times (2 \times 20 \times 10^{-4})}{4\pi \times 10^{-7}} = \underline{\underline{2292 \text{ N}}}$$

3.
(a)

Parameters of transformer:

- Parallelelements: R_o and X_o
- Series elements: R_T and X_T



Open circuit test

- Apply $V_1 = \text{rated voltage}$
 - All current is in the parallel elements
- Measure V_1 , I_1 , and P_1

$$P_1 = \frac{V_1^2}{R_o} \rightarrow R_o$$

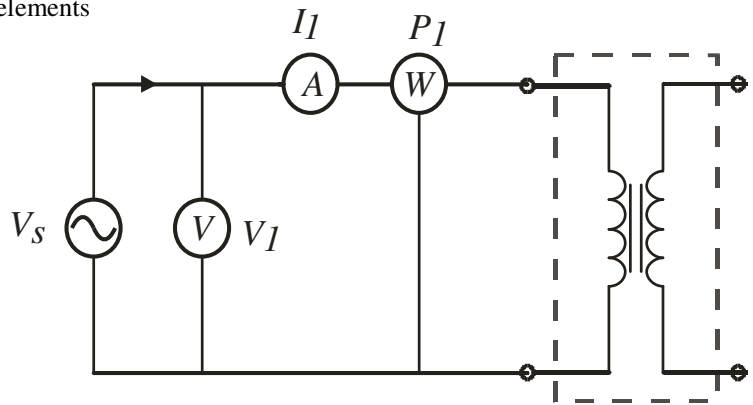
$$I_{Loss} = \frac{V_1}{R_o}$$

$$I_o = \frac{P_1}{V_1}$$

$$I_{mag}^2 + I_{Loss}^2 = I_o^2$$

$$X_o = \frac{V_1}{I_{mag}}$$

Gives X_o



Short circuit test

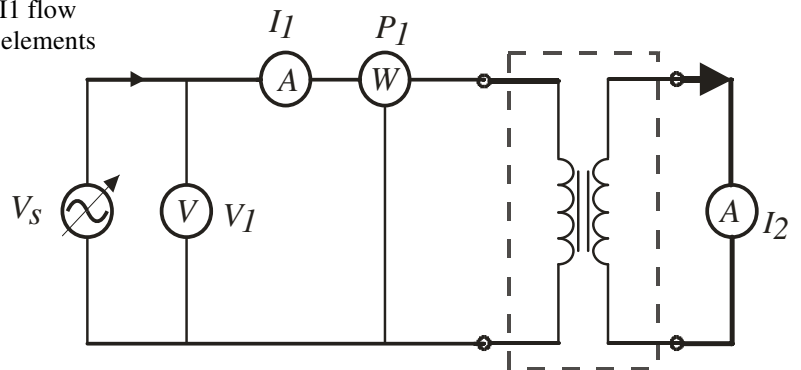
- Apply low V_1 gradually until rated I_1 flow
 - All current is in the series elements
- Measure V_1 , I_1 , and P_1

$$I_1^2 R_T = P_1$$

$$Z_T = \frac{V_1}{I_1}$$

$$Z_T^2 = R_T^2 + X_T^2$$

Gives R_T and X_T



(b)

$$(i) R_T = \frac{P_1}{I_1^2} = \frac{202}{4.17^2} = \underline{\underline{11.6 \Omega}}$$

$$Z_T = \frac{V_1}{I_1} = \frac{138}{4.17} = 33.1 \Omega$$

$$X_T = \sqrt{Z_T^2 - R_T^2} = \sqrt{33.1^2 - 11.6^2} = \underline{\underline{31 \Omega}}$$

$$\varphi_T = \tan^{-1} \frac{X_T}{R_T} = \tan^{-1} \frac{31}{11.6} = \tan^{-1} 2.67 = 69.5^\circ$$

$$\varphi_L = \cos^{-1} 0.866 = 30^\circ$$

$$(ii) I_{2FL}' = I_{1FL} = \frac{S_r}{V_1} = \frac{10 \times 10^3}{2400} = 4.17 \text{ A}$$

$$\text{Re } g = \frac{I_2' Z_T}{V_1} \cos(\varphi_T - \varphi_L) = \frac{(0.8 \times 4.17) \times 33.1}{2400} \cos(30^\circ - 69.5^\circ) = 0.035 = \underline{\underline{3.5\%}}$$

4.

(a)

- In three phase power is constant from the prime to the load, while in single phase it fluctuates at twice the supply frequency
- There is a saving in transmission conductors from 6 in single phase to 3 or 4 in three phase
- The specific output (power unit volume) of three phase machines is higher than for single phase machines

(b)

$$P_1 = (v_a i_a) \big|_{AV} = (v_a - v_b) i_a \big|_{AV}$$

$$P_2 = (v_b i_b) \big|_{AV} = (v_b - v_c) i_b \big|_{AV}$$

$$P_1 + P_2 = (v_a i_a) \big|_{AV} + (v_b i_b) \big|_{AV} - v_c (i_a + i_b) \big|_{AV}$$

if there is no neutral

$$i_a + i_b + i_c = 0$$

And therefore

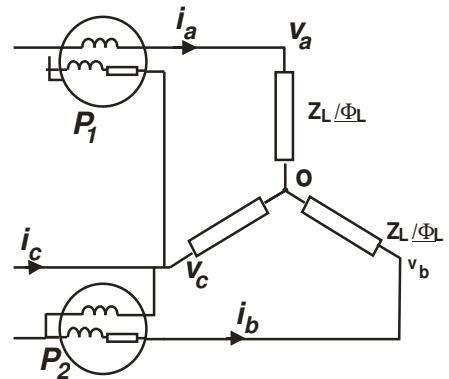
$$P_1 + P_2 = (v_a i_a) \big|_{AV} + (v_b i_b) \big|_{AV} + (v_c i_c) \big|_{AV}$$

$$P_1 + P_2 = P_a + P_b + P_c$$

(c)

$$V_L = 400 \text{ V}, I_L = 20 \text{ A}, P_T = 20 \text{ kW}.$$

$$(i) p.f. = \cos \varphi_L = \frac{P_T}{\sqrt{3} V_L I_L} = \frac{12 \times 10^3}{\sqrt{3} \times 400 \times 20} = \underline{\underline{0.866}}$$



$$Z_L = \frac{V_p}{I_p} = \frac{V_L/\sqrt{3}}{I_L} = \frac{400/\sqrt{3}}{20} = 11.55 \, \Omega$$

$$\cos^{-1} \phi_L = 30^\circ$$

$$Z_L = 11.55/\underline{30^\circ} \, \Omega = \underline{\underline{10 + j5.775 \, \Omega}}$$

(ii)

$$P_1 + P_2 = 12 \times 10^3$$

$$P_1 - P_2 = V_L I_L \sin \phi_L = 400 \times 20 \times \sin 30^\circ = 4 \times 10^3$$

$$2P_1 = 16 \times 10^3 \Rightarrow P_1 = \underline{\underline{8 \times 10^3 \, \text{W}}}$$

$$P_2 = (8 - 4) \times 10^3 = \underline{\underline{4 \times 10^3 \, \text{W}}}$$

5.

(a)

DC Shunt

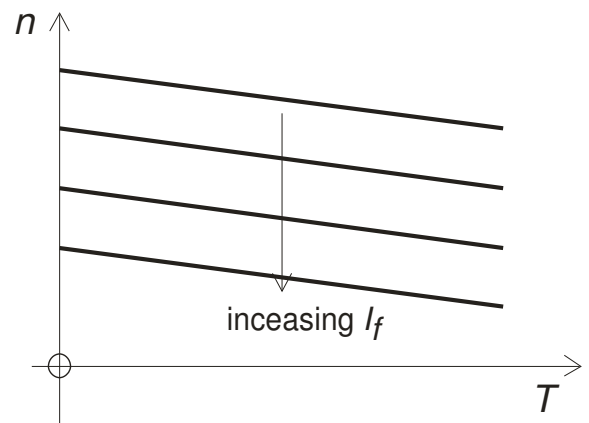
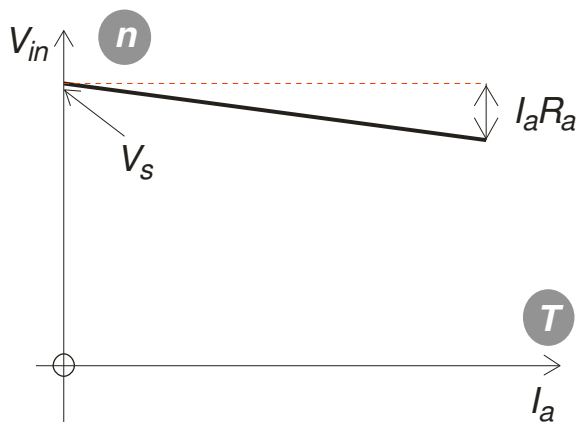
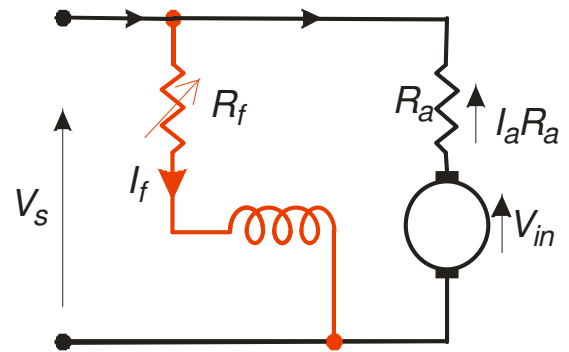
$$V_s = V_{in} + I_a R_a$$

$$T = \frac{1}{2\pi} \left(\frac{2pZ}{c} \right) \phi I_a$$

At constant field current (and therefore constant flux)

$$V_{in} \propto n$$

$$T \propto I_a$$



DC Series

$$I_s = I_a = I_f = I$$

Two assumptions:

- Neglect IR drops
- Neglect saturation

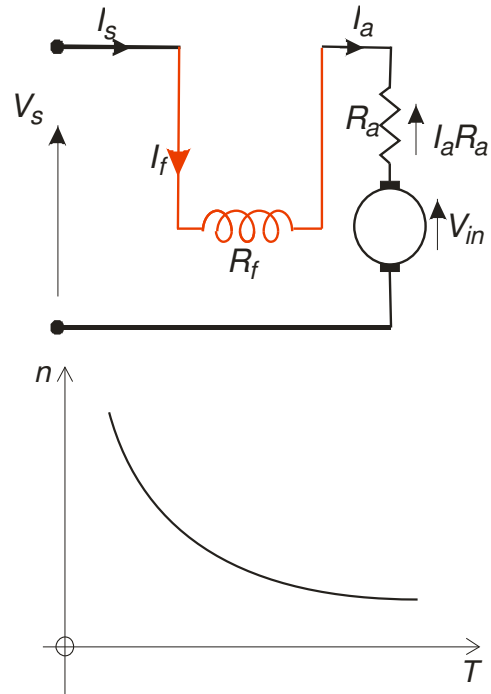
$$V_s = V_{in} = \left(\frac{2pZ}{c} \right) n \phi$$

$$\therefore n \propto \frac{1}{\phi} \propto \frac{1}{I}$$

$$T = \frac{1}{2\pi} \left(\frac{2pZ}{c} \right) \phi I_a$$

$$T \propto I^2$$

$$T \propto \frac{1}{n^2}$$



(b)

$V_s = 240 \text{ V}$, $n_1 = 800 \text{ r/min}$, $I_{a1} = 0$, $R_f = 160 \text{ } \Omega$, $R_a = 0.4 \text{ } \Omega$; $n_2 = 950 \text{ r/min}$, $I_{a2} = 20 \text{ A}$.

$$V_{in1} = k n_1 \phi_1 = 240$$

$$k \phi_1 = \frac{240}{n_1} = \frac{240}{800} \propto I_{f1}$$

$$V_{in2} = V_s - I_a R_a = 240 - 20 \times 0.4 = 232$$

$$k n_2 \phi_2 = 232$$

$$k \phi_2 = \frac{232}{n_2} = \frac{232}{950} \propto I_{f2}$$

$$I_{f2} = \frac{232}{950} \cdot \frac{800}{240} I_f = \frac{232}{950} \cdot \frac{800}{240} \frac{V_s}{R_{f1}} = \frac{232}{950} \cdot \frac{800}{240} \cdot \frac{240}{160} = 0.814 \text{ A}$$

$$R_{f2} = \frac{V_s}{I_{f2}} = \frac{240}{0.814} = 295 \text{ } \Omega$$

$$R_{ex} = R_{f2} - 160 = 295 - 160 = \underline{\underline{135 \text{ } \Omega}}$$

6.

(a)

$$F_y = \frac{\sqrt{3}}{2}(F_2 - F_3)$$

$$= \frac{\sqrt{3}}{2}NI_m \left[\overline{\cos \omega t - 120^\circ} - \overline{\cos \omega t + 120^\circ} \right]$$

$$= \frac{\sqrt{3}}{2}NI_m 2 \sin \omega t \sin 120^\circ$$

$$F_y = \frac{3}{2}NI_m \sin \omega t$$

$$i_1 = I_m \cos \omega t$$

$$i_2 = I_m \overline{\cos \omega t - 120^\circ}$$

$$i_3 = I_m \overline{\cos \omega t + 120^\circ}$$

$$F_1 = NI_m \cos \omega t$$

$$F_2 = NI_m \overline{\cos \omega t - 120^\circ}$$

$$F_3 = NI_m \overline{\cos \omega t + 120^\circ}$$

$$F_x = F_1 - \frac{1}{2}(F_2 + F_3)$$

$$= NI_m \left[\cos \omega t - \frac{1}{2}(\overline{\cos \omega t - 120^\circ} + \overline{\cos \omega t + 120^\circ}) \right]$$

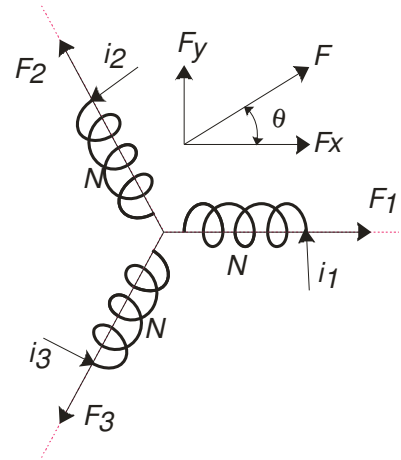
$$= NI_m \left[\cos \omega t - \frac{1}{2}2 \cos \omega t \cos 120^\circ \right]$$

$$F_x = \frac{3}{2}NI_m \cos \omega t$$

$$|F| = \sqrt{F_x^2 + F_y^2} = \underline{\underline{\frac{3}{2}NI_m}}$$

$$\tan \theta = \frac{F_y}{F_x} = \tan \omega t$$

$$\underline{\underline{\theta = \omega t}}$$



(b)

Synchronous machine:

Rotor has field winding excited by dc current; rotor speed is constant and equal to speed of rotating flux

Induction machine:

Rotor has windings short-circuited on themselves and are unexcited; rotor slips so its speed is a little less than the speed of the rotating magnetic flux

(c)

F = 50 Hz, p = 3, VS = 220 V, NS = 2NR

$$(i) \ s = \frac{f_R}{f} = \frac{2}{50} = \underline{\underline{0.04}}$$

$$(ii) \ n = n_s (1 - s) = \frac{f}{p} (1 - s) = \frac{50}{3} (1 - 0.04) = 16 \text{ r/s} = \underline{\underline{960 \text{ r/min}}}$$

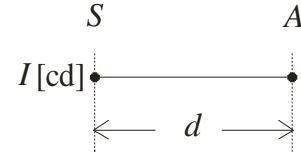
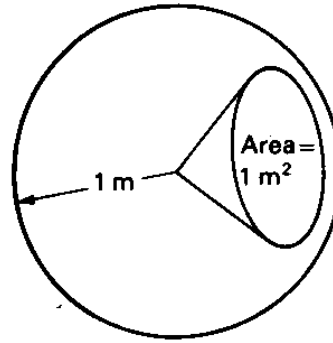
$$(iii) \ E_R = \frac{N_R}{N_s} s E_s = \frac{1}{2} \times 0.04 \times 220 = \underline{\underline{4.4 \text{ V}}}$$

7.
(a)

Inverse square law:

$$\frac{E_{\text{at } r}}{E_{\text{at 1 m radius}}} = \frac{\phi/4\pi r^2}{\phi/4\pi} = \frac{4\pi}{4\pi r^2} = \frac{1}{r^2}$$

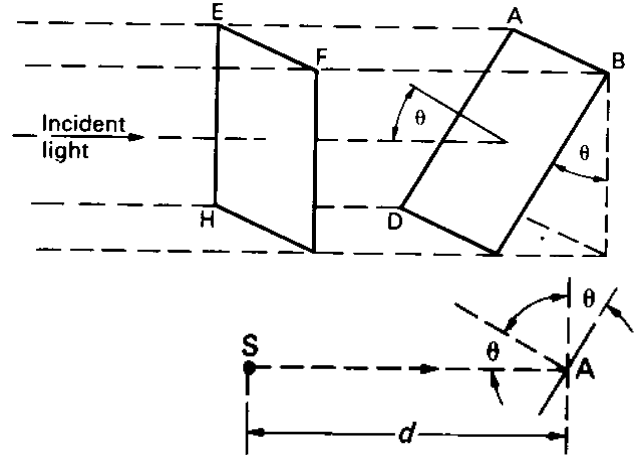
$$E_A = \frac{I}{d^2}$$



Cosine law of illumination:

$$\frac{E_{ABCD}}{E_{EFGH}} = \frac{\phi/S_{ABCD}}{\phi/S_{EFGH}} = \frac{S_{EFGH}}{S_{ABCD}} = \cos \theta$$

$$E_A = \frac{I}{d^2} \cos \theta$$



(b)

EA = 20 lx, IA = 500 dc, d = 1 m, d1 = 9m, d2 = ?

$$E_A = \frac{I_A}{d_1^2} + \frac{I_B}{d_2^2} \cos \theta$$

$$d_2^2 = 9^2 + 1^2 = 82$$

$$\cos \theta = \frac{9}{\sqrt{9^2 + 1^2}} = 0.99$$

$$I_B = \left(E_A - \frac{I_A}{d_1^2} \right) \frac{d_2^2}{\cos \theta} = \left(20 - \frac{500}{9^2} \right) \frac{82}{0.99} = \underline{\underline{1145 \text{ cd}}}$$

(c) A = 14 x 12 = 144 m², E = 80 lx, UF = 0.5, MF = 0.8, Eff. = 14.75 lm/W, P = 100 W.

$$\phi_{\text{total}} = \frac{EA}{UF \times UF} = \frac{12 \times 12 \times 80}{0.5 \times 0.8} = 28,800 \text{ lm}$$

$$P_{\text{total}} = \frac{\phi_{\text{total}}}{\text{Eff.}} = \frac{28800}{14.75} = 1955 \text{ W}$$

$$N = \frac{1955}{100} = 19.55 \approx \underline{\underline{20 \text{ lamps}}}$$