

EEE 3351

ELECTROMECHANICS & ELECTRICAL MACHINES

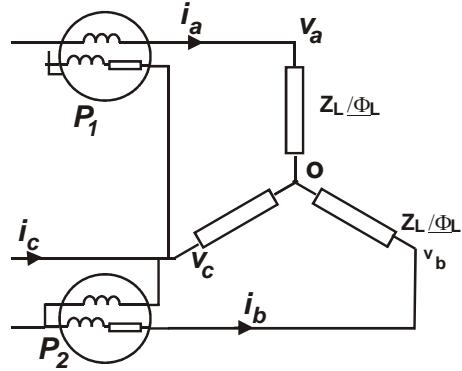
UNIVERSITY EXAMINATIONS

FEBRUARY/MARCH 2014

MODEL SOLUTIONS

4.

(a)



$$P_1 = (v_a i_a)|_{AV} = (v_a - v_b)i_a|_{AV}$$

$$P_2 = (v_b i_b)|_{AV} = (v_b - v_c)i_b|_{AV}$$

$$P_1 + P_2 = (v_a i_a)|_{AV} + (v_b i_b)|_{AV} - v_c (i_a + i_b)|_{AV}$$

if there is no neutral

$$i_a + i_b + i_c = 0$$

And therefore

$$P_1 + P_2 = (v_a i_a)|_{AV} + (v_b i_b)|_{AV} + (v_c i_c)|_{AV}$$

$$P_1 + P_2 = P_a + P_b + P_c$$

(b)

$V_L = 380 \text{ V}$, $S_1 = 5 \text{ kVA}$, $S_2 = 10 \text{ kVA}$, $\text{pf}_1 = 0.8$, $\text{p.f.}_2 = 0.9$. 20 A , $P_T = 20 \text{ kW}$.

$$S_1 = 4000 + j3000$$

$$S_2 = 9000 + j4350$$

$$S_T = 13000 + j7350 = 14900/\underline{29.5^\circ}$$

$$I_L = \frac{S_T}{\sqrt{3}V_L} = \frac{14900}{\sqrt{3} \times 380} = \underline{\underline{22.6 \text{ A}}}$$

$$P_1 + P_2 = 13 \times 10^3$$

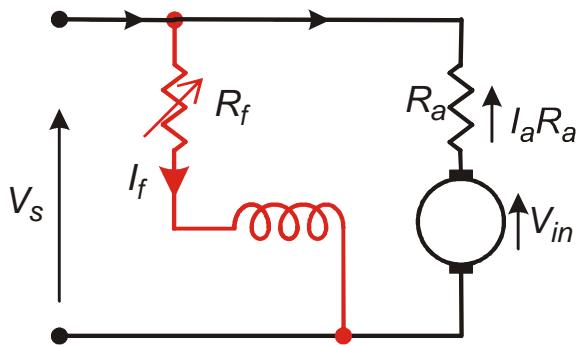
$$P_1 - P_2 = V_L I_L \sin \varphi_L = 380 \times 22.6 \times \sin 29.6^\circ = 4.2 \times 10^3$$

$$2P_1 = 17.2 \times 10^3 \Rightarrow P_1 = \underline{\underline{8.6 \times 10^3 \text{ W}}}$$

$$P_2 = (13 - 8.6) \times 10^3 = \underline{\underline{4.4 \times 10^3 \text{ W}}}$$

5.

(a)

DC Shunt

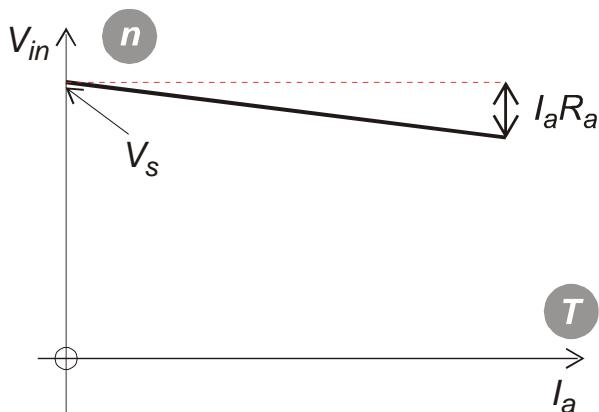
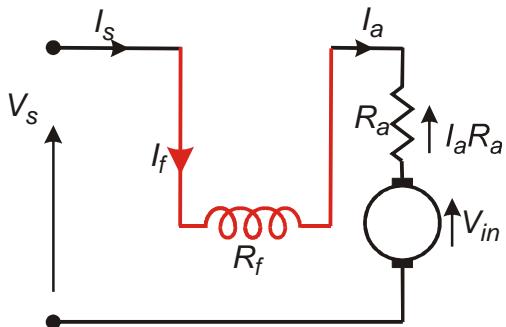
$$V_s = V_{in} + I_a R_a$$

$$T = \frac{1}{2\pi} \left(\frac{2pZ}{c} \right) \phi I_a$$

At constant field current (and therefore constant flux)

$$V_{in} \propto n$$

$$T \propto I_a$$

**DC Series**

$$I_s = I_a = I_f = I$$

Two assumptions:

- Neglect IR drops
- Neglect saturation

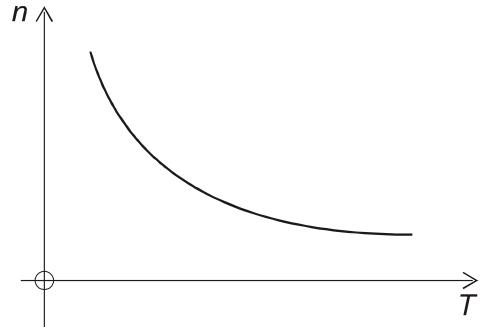
$$V_s = V_{in} = \left(\frac{2pZ}{c} \right) n\phi$$

$$\therefore n \propto \frac{1}{\phi} \propto \frac{1}{I}$$

$$T = \frac{1}{2\pi} \left(\frac{2pZ}{c} \right) \phi I_a$$

$$T \propto I^2$$

$$T \propto \frac{1}{n^2}$$



(b)

$$V_s = 400 \text{ V}, I_s = 50 \text{ A}, I_f = 2 \text{ A}, n = 1000 \text{ r/min}, R_a = 0.5 \Omega, P_{W+F} = 600 \text{ W}.$$

$$I_a = I_s - I_f = 50 - 2 = 48 \text{ A}$$

$$P_{Cu} = V_f I_f + I_a^2 R_a = 400 \times 2 + 48^2 \times 0.5 = 200 + 1152 = 1352 \text{ W}$$

$$P_{Loss} = P_{Cu} + P_{W+F} = 1352 + 600 = \underline{\underline{1852 \text{ W}}}$$

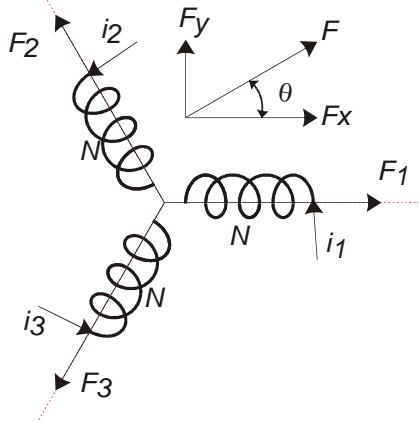
$$\eta = 1 - \frac{P_{Loss}}{P_{in}} = 1 - \frac{1850}{400 \times 50} = 0.9074 = \underline{\underline{90.7\%}}$$

$$P_{out} = 20000 - 1852 = 18148$$

$$T = \frac{P_{out}}{2\pi n} = \frac{18148}{2\pi \times 1000 / 60} = \underline{\underline{173.3 \text{ Nm}}}$$

6.

(a)



$$\begin{aligned}
 F_y &= \frac{\sqrt{3}}{2} (F_2 - F_3) \\
 &= \frac{\sqrt{3}}{2} NI_m \left[\cos \overline{\omega t - 120^\circ} - \cos \overline{\omega t + 120^\circ} \right] \\
 &= \frac{\sqrt{3}}{2} NI_m 2 \sin \omega t \sin 120^\circ
 \end{aligned}$$

$$F_y = \frac{3}{2} NI_m \sin \omega t$$

$$i_1 = I_m \cos \omega t$$

$$i_2 = I_m \cos \underline{\omega t - 120^\circ}$$

$$i_3 = I_m \cos \underline{\omega t + 120^\circ}$$

$$F_1 = NI_m \cos \omega t$$

$$F_2 = NI_m \cos \underline{\omega t - 120^\circ}$$

$$F_3 = NI_m \cos \underline{\omega t + 120^\circ}$$

$$\begin{aligned}
 F_x &= F_1 - \frac{1}{2} (F_2 + F_3) \\
 &= NI_m \left[\cos \omega t - \frac{1}{2} (\cos \underline{\omega t - 120^\circ} + \cos \underline{\omega t + 120^\circ}) \right] \\
 &= NI_m \left[\cos \omega t - \frac{1}{2} 2 \cos \omega t \cos 120^\circ \right]
 \end{aligned}$$

$$F_x = \frac{3}{2} NI_m \cos \omega t$$

$$|F| = \sqrt{F_x^2 + F_y^2} = \underline{\underline{\frac{3}{2} NI_m}}$$

$$\tan \theta = \frac{F_y}{F_x} = \tan \omega t$$

$$\underline{\underline{\theta = \omega t}}$$

(b)

$f = 50 \text{ Hz}$, $p = 3$, $f_R = 4 \text{ Hz}$

$$(i) s = \frac{f_R}{f} = \frac{4}{50} = \underline{\underline{0.08}}$$

$$(ii) n = n_s(1-s) = \frac{f}{p}(1-s) = \frac{50}{3}(1-0.08) = 15.33 \text{ r/s} = \underline{\underline{920 \text{ r/min}}}$$

(iii) 80 r/min, 920 r/min

(c)

Synchronous machine:

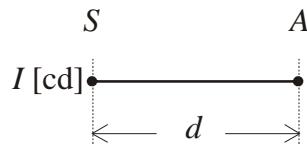
Rotor has field winding excited by dc current; rotor speed is constant and equal to speed of rotating flux

Induction machine:

Rotor has windings short-circuited on themselves and are unexcited; rotor slips so its speed is a little less than the speed of the rotating magnetic flux

7.

(a)

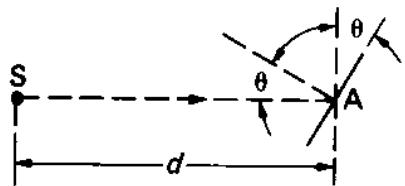


Inverse square law:

$$\frac{E_{at} r}{E_{at} \text{ 1 m radius}} = \frac{\phi / 4\pi r^2}{\phi / 4\pi} = \frac{4\pi}{4\pi r^2} = \frac{1}{r^2}$$

$$E_A = \frac{I}{d^2}$$

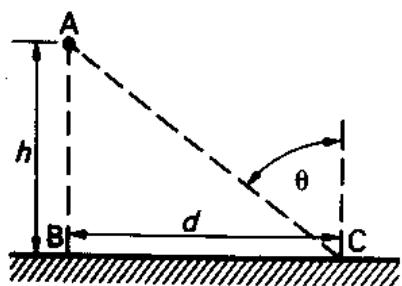
Cosine law of illumination:



$$\frac{E_{ABCD}}{E_{EFGH}} = \frac{\phi / S_{ABCD}}{\phi / S_{EFGH}} = \frac{S_{EFGH}}{S_{ABCD}} = \cos \theta$$

$$E_A = \frac{I}{d^2} \cos \theta$$

(b)



$$AC = \sqrt{h^2 + d^2}$$

$$\cos \theta = \frac{h}{\sqrt{h^2 + d^2}}$$

$$E_B = \frac{I_{AB}}{h^2}$$

$$E_C = \frac{I_{AC} \cos \theta}{AC^2} = I_{AC} \cdot \frac{h}{\left(h^2 + d^2\right)^{\frac{3}{2}}}$$

Assume that, in the lower hemisphere, the luminous intensity is uniform

$$I_{AB} = I_{AC} = I$$

$$I = E_B \cdot h^2$$

$$I = E_C \cdot \frac{\left(h^2 + d^2\right)^{\frac{3}{2}}}{h}$$

$$E_C = E_B \cdot \frac{h^3}{\left(h^2 + d^2\right)^{\frac{3}{2}}} = E_B \left[\frac{h}{\left(h^2 + d^2\right)^{\frac{1}{2}}} \right]^3 = E_B \cos^3 \theta$$

$$E_C = E_B \cos^3 \theta$$

(c)

$$E_{AV} = 400 \text{ lx}$$

Lamp above A = O

Corner of court = A

Centre of court = B

θ = angle AOB

$$\cos \theta = \frac{7}{\sqrt{7^2 + 500}} = 0.2987$$

$$E_{BO} = \frac{400}{4} = 100 \text{ lx}$$

$$E_B = E_A \cos^3 \theta \rightarrow E_A = \frac{E_B}{\cos^3 \theta} = \frac{100}{0.2978^3} = 37,523 \text{ lx}$$

$$I = E_A d^2 = 37,523 \times 7^2 = 183,861 \text{ cd}$$

$$\phi_{lamp} = 4\pi \times 183,861 = 2,310,465 \text{ lm}$$

(i)

$$N = \frac{2,310,465}{2500} \approx \underline{\underline{92 \text{ lamps}}}$$

(ii)

$$N = \frac{2,310,465 \times 0.4}{2500} \approx \underline{\underline{37 \text{ lamps}}}$$