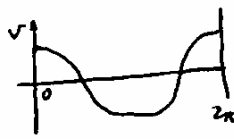


4. (a) $V = Blv$

$\oint \frac{1}{l} dx$



$$V_{av} = \frac{\int_0^t Blv dt}{t} = \frac{\int_0^t Bl dx}{t} = \frac{\int_0^t \delta \phi}{t}$$

ϕ = total flux / pole

Integrating over 1 pole-pitch $\int \delta \phi = \phi$

t = time for 1 pole pitch = $\frac{1}{2n}$; $V_{av} = \frac{\phi}{\frac{1}{2n}} = 2n\phi$

For a m/c with p pairs of poles $V_{av} = 2np\phi$

If rotor has Z conductors in parallel and there are C paths then $Z_s = \frac{Z}{C}$ = number of series connected conductors.

For commutator m/c output is dc = average induced voltage = $V = \frac{2pZ}{C} n \phi$

For slip ring m/c output is ac and if sinusoidal waveform is assumed then form factor is 1.11. Thus rms output is $2pZ_s n \phi \times 1.11$ and taking into account the winding factor k $V = 2.22 p Z_s n \phi k$ at freq f $f = np$; $V = 2.22 Z_s f \phi k$.

[10]

(b) $p = 3$

$\phi = 0.06 \text{ Wb}$

$Z = 664$

$n = 250 \text{ rpm}$

$V = \frac{2pZ}{C} n \phi = 2 \times 3 \times \frac{664}{2} \times \frac{250}{60} \times 0.06 = 498 \text{ V}$

For $\phi' = 0.058$ and $V = 250 \text{ V}$

$n = \frac{V \cdot C}{2pZ\phi} = \frac{250 \times 2}{2 \times 3 \times 664 \times 0.058} \text{ rev/s}$

$= 130 \text{ rpm}$

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