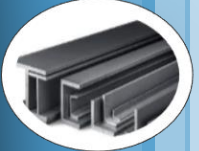


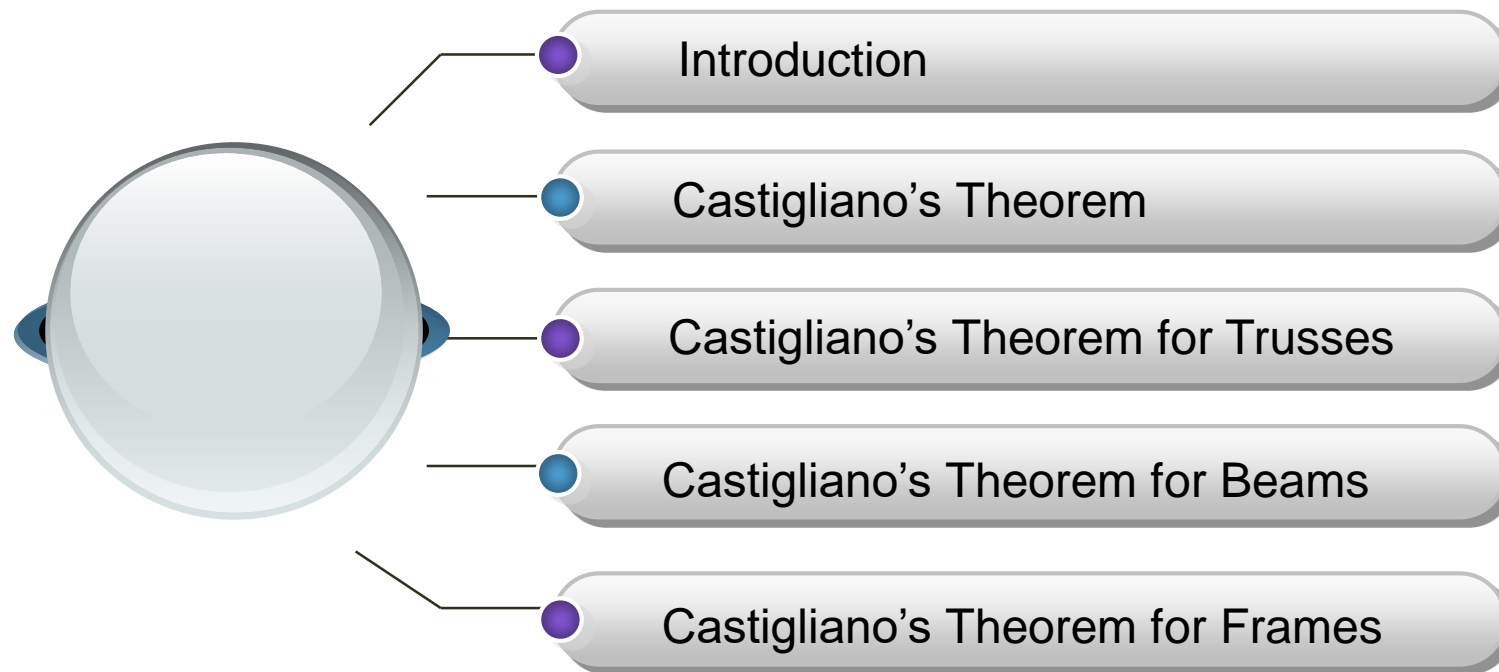
CEE 3222: THEORY OF STRUCTURES

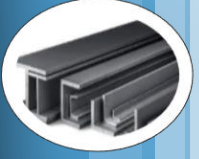
Lecture 3.3

ENERGY METHODS - CASTIGLIANO's THEOREMS



Contents

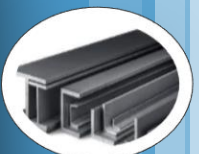




Introduction

- All energy methods are based on the conservation of energy principle, which states that the work done by all external forces acting on the structure, U_e , is transformed into internal work or strain energy, U_i , developed in the members when the structure deforms.

$$U_e = U_i$$



Castigliano's Theorem

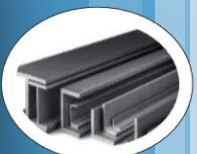
- This method is also called *Castigliano's second theorem*, or the **method of least work**.
- *It states that the displacement (slope) of a point is equal to the first partial derivative of the strain energy in the structure with respect to a force (couple moment) acting at the point and in the direction of displacement*

$$\Delta_i = \frac{\partial U_i}{\partial P_i}$$

Assumptions on structures.

1. constant temperature
2. unyielding supports
3. linear elastic material response.

- The equation is a statement regarding the structure's compatibility.
- The above derivation requires that only conservative forces be considered for the analysis.
- These forces do work that is independent of the path and therefore create no energy loss.



Castigliano's Theorem for Trusses

- Recall that the strain energy for an axial force is given by

$$U_i = \frac{N^2 L}{2AE}$$

- Substituting this in $\Delta_i = \frac{\partial U_i}{\partial P_i}$

- We get formula using the theorem

$$\Delta = \sum N \left(\frac{\partial N}{\partial P} \right) \frac{L}{AE}$$

where

Δ = external joint displacement of the truss.

P = external force applied to the truss joint in the direction of Δ .

N = internal force in a member caused by *both* the force P and the loads on the truss.

L = length of a member.

A = cross-sectional area of a member.

E = modulus of elasticity of a member.

- Each member force N must be expressed as a function of P .

Castigliano's Theorem for Trusses

Procedure for Analysis

The following procedure provides a method that may be used to determine the displacement of any joint of a truss using Castigliano's theorem.

External Force P

- Place a force P on the truss at the joint where the desired displacement is to be determined. This force is assumed to have a *variable magnitude* in order to obtain the change $\partial N / \partial P$. Be sure \mathbf{P} is directed along the line of action of the displacement.

Internal Forces N

- Determine the force N in each member caused by both the real (numerical) loads and the variable force P . Assume tensile forces are positive and compressive forces are negative.
- Compute the respective partial derivative $\partial N / \partial P$ for each member.

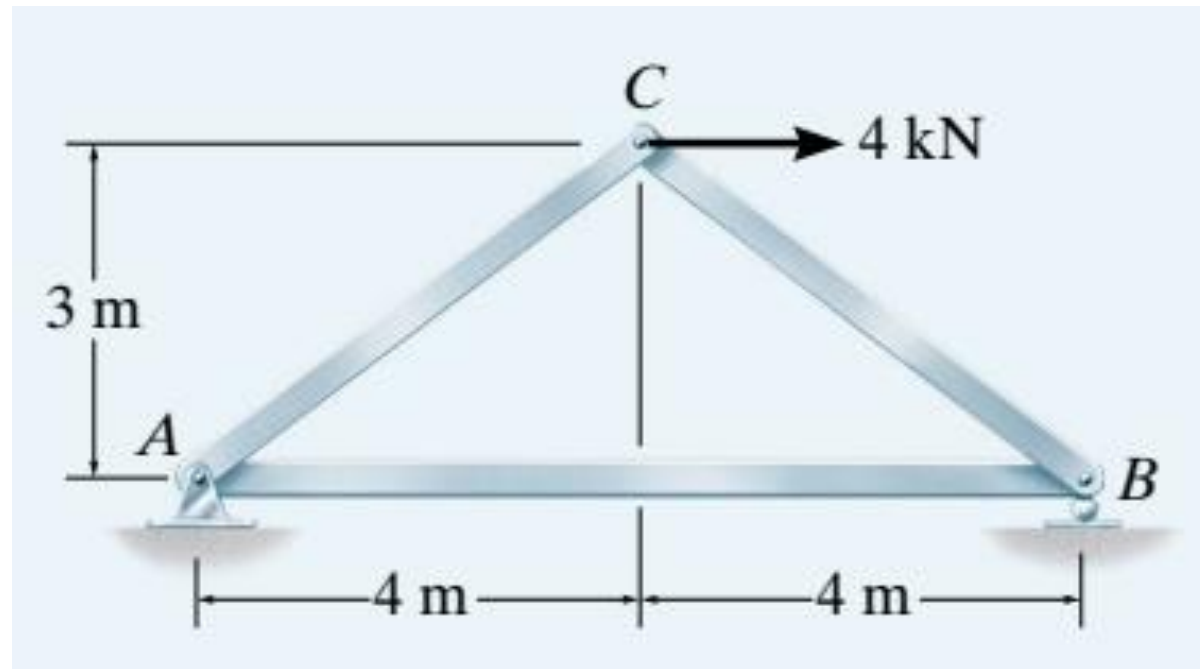
- After N and $\partial N / \partial P$ have been determined, assign P its numerical value if it has replaced a real force on the truss. Otherwise, set P equal to zero.

Castigliano's Theorem

- Apply Castigliano's theorem to determine the desired displacement Δ . It is important to retain the algebraic signs for corresponding values of N and $\partial N / \partial P$ when substituting these terms into the equation.
- If the resultant sum $\sum N(\partial N / \partial P)L / AE$ is positive, Δ is in the same direction as P . If a negative value results, Δ is opposite to P .

Example 1

- Determine the vertical displacement of joint C of the truss shown in the figure. The cross-sectional area of each member is $A = 400\text{mm}^2$ and $E = 200\text{ GPa}$



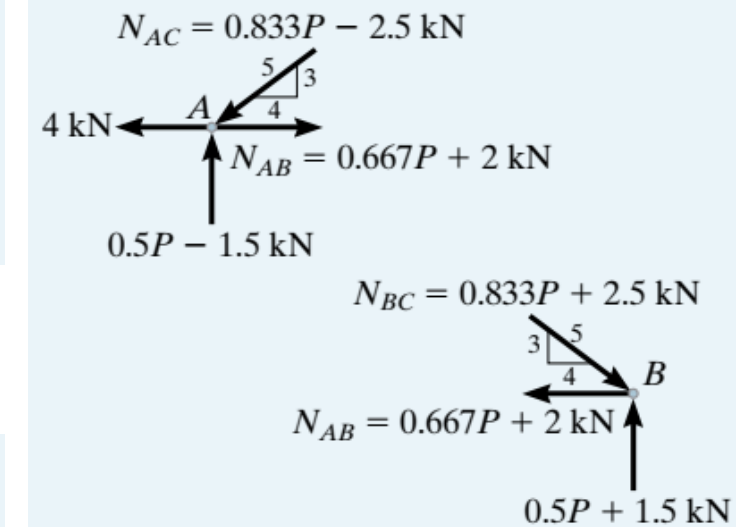
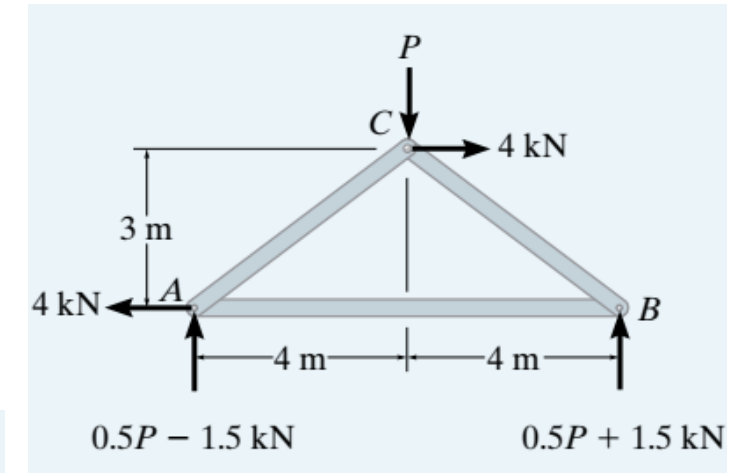
Solution 1

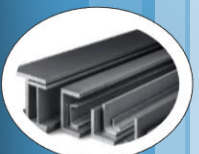
- A vertical force P is applied to the truss at joint C , since this is where the vertical displacement is to be determined
- Since P does not actually exist as a real load on the truss, we require $P = 0$ in the table below

Member	N	$\frac{\partial N}{\partial P}$	$N(P = 0)$	L	$N\left(\frac{\partial N}{\partial P}\right)L$
AB	$0.667P + 2$	0.667	2	8	10.67
AC	$-(0.833P - 2.5)$	-0.833	2.5	5	-10.42
BC	$-(0.833P + 2.5)$	-0.833	-2.5	5	10.42
					$\Sigma = 10.67 \text{ kN} \cdot \text{m}$

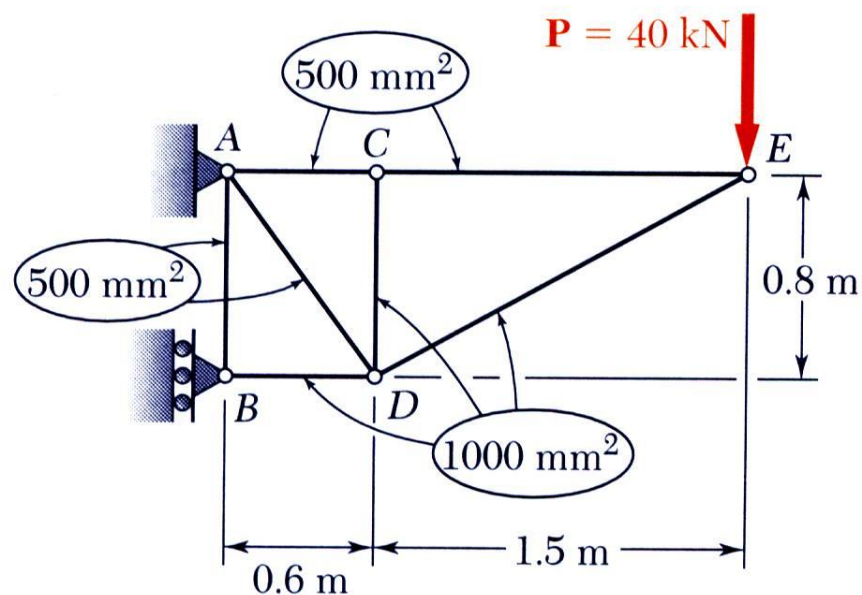
$$\Delta_{C_v} = \sum N \left(\frac{\partial N}{\partial P} \right) \frac{L}{AE} = \frac{10.67 \text{ kN} \cdot \text{m}}{AE}$$

$$\Delta_{C_v} = \frac{10.67(10^3) \text{ N} \cdot \text{m}}{400(10^{-6}) \text{ m}^2 (200(10^9) \text{ N/m}^2)} = 0.000133 \text{ m} = 0.133 \text{ mm} \quad \text{Ans.}$$





Example 2 + Solution



Members of the truss shown consist of sections of aluminum pipe with the cross-sectional areas indicated. Using $E = 73 \text{ GPa}$, determine the vertical deflection of the joint C caused by the load P .

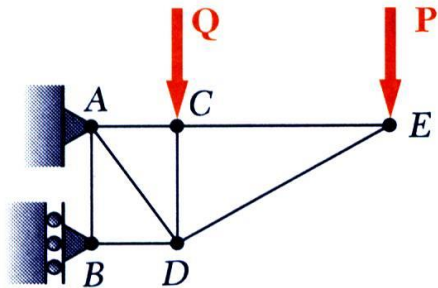
SOLUTION:

- For application of Castigliano's theorem, introduce a dummy vertical load Q at C . Find the reactions at A and B due to the dummy load from a free-body diagram of the entire truss.
- Apply the method of joints to determine the axial force in each member due to Q .
- evaluate the derivative with respect to Q of the strain energy of the truss due to the loads P and Q .
- Setting $Q = 0$, evaluate the derivative which is equivalent to the desired displacement at C .

Solution 2

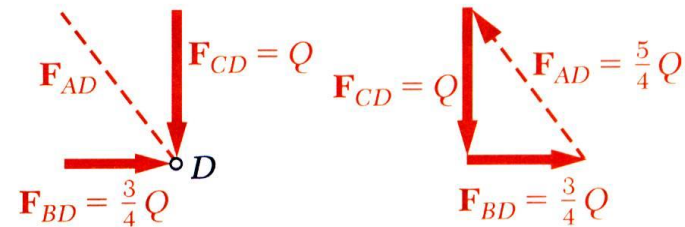
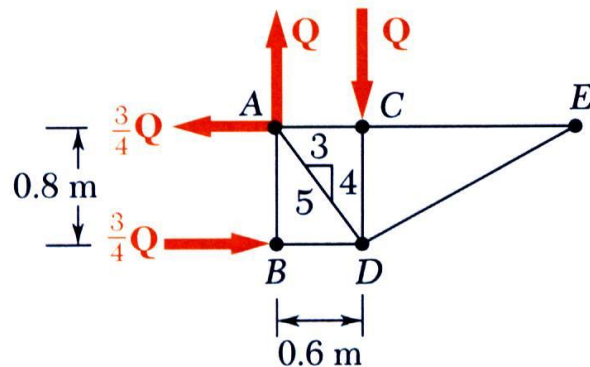
SOLUTION:

- Find the reactions at A and B due to a dummy load Q at C from a free-body diagram of the entire truss.



$$A_x = -\frac{3}{4}Q \quad A_y = Q \quad B = \frac{3}{4}Q$$

- Apply the method of joints to determine the axial force in each member due to Q .

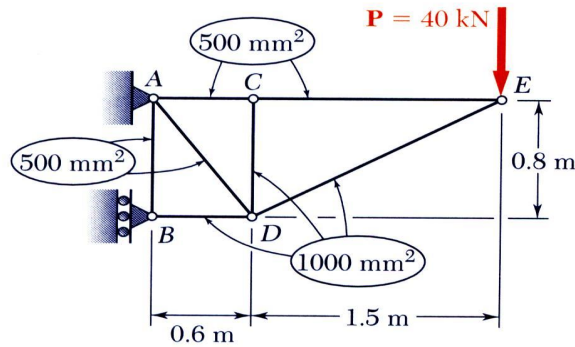


$$F_{CE} = F_{DE} = 0$$

$$F_{AC} = 0; F_{CD} = -Q$$

$$F_{AB} = 0; F_{BD} = -\frac{3}{4}Q$$

Solution 2



Member	F_i	$\partial F_i / \partial Q$	L_i, m	A_i, m^2	$\left(\frac{F_i L_i}{A_i} \right) \frac{\partial F_i}{\partial Q}$
AB	0	0	0.8	500×10^{-6}	0
AC	$+15P/8$	0	0.6	500×10^{-6}	0
AD	$+5P/4 + 5Q/4$	$\frac{5}{4}$	1.0	500×10^{-6}	$+3125P + 3125Q$
BD	$-21P/8 - 3Q/4$	$-\frac{3}{4}$	0.6	1000×10^{-6}	$+1181P + 338Q$
CD	$-Q$	-1	0.8	1000×10^{-6}	$+800Q$
CE	$+15P/8$	0	1.5	500×10^{-6}	0
DE	$-17P/8$	0	1.7	1000×10^{-6}	0

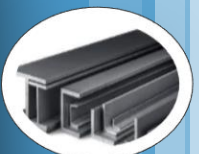
- Combine with the results of Sample Problem 11.4 to evaluate the derivative with respect to Q of the strain energy of the truss due to the loads P and Q .

$$y_C = \sum \left(\frac{F_i L_i}{A_i E} \right) \frac{\partial F_i}{\partial Q} = \frac{1}{E} (4306P + 4263Q)$$

- Setting $Q = 0$, evaluate the derivative which is equivalent to the desired displacement at C.

$$y_C = \frac{4306(40 \times 10^3 \text{ N})}{73 \times 10^9 \text{ Pa}}$$

$$y_C = 2.36 \text{ mm} \downarrow$$



Castigliano's Theorem for Beams and Frames

- The internal bending strain energy for a beam or frame is given by $U_i = \int M^2 dx / 2EI$. Substituting this equation into $\Delta_i = \partial U_i / \partial P_i$ and omitting the subscript i , we have

$$\Delta = \frac{\partial}{\partial P} \int_0^L \frac{M^2 dx}{2EI}$$

where

Δ = external displacement of the point caused by the real loads acting on the beam or frame.

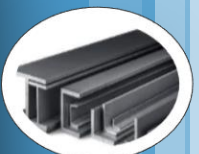
P = external force applied to the beam or frame in the direction of Δ .

M = internal moment in the beam or frame, expressed as a function of x and caused by both the force P and the real loads on the beam.

E = modulus of elasticity of beam material.

I = moment of inertia of cross-sectional area computed about the neutral axis.

$$\Delta = \int_0^L M \left(\frac{\partial M}{\partial P} \right) \frac{dx}{EI}$$



Castigliano's Theorem for Beams and Frames

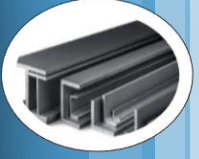
- If the slope θ at a point is to be determined, we must find the partial derivative of the internal moment M with respect to an external couple moment M' acting at the point.

$$\theta = \int_0^L M \left(\frac{\partial M}{\partial M'} \right) \frac{dx}{EI}$$

- For shear and torsion, we have the following and their partial derivative.

$$U_s = K \int_0^L \frac{V^2 dx}{2AG} \quad \frac{\partial U_s}{\partial P} = \int_0^L \frac{V}{AG} \left(\frac{\partial V}{\partial P} \right) dx$$

$$U_t = \int_0^L \frac{T^2 dx}{2JG} \quad \frac{\partial U_t}{\partial P} = \int_0^L \frac{T}{JG} \left(\frac{\partial T}{\partial P} \right) dx$$



Castigliano's Theorem for Beams and Frames

Procedure for Analysis

The following procedure provides a method that may be used to determine the deflection and/or slope at a point in a beam or frame using Castigliano's theorem.

External Force P or Couple Moment M'

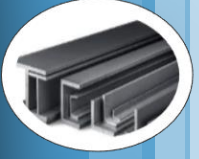
- Place a force \mathbf{P} on the beam or frame at the point and in the direction of the desired displacement.
- If the slope is to be determined, place a couple moment \mathbf{M}' at the point.
- It is assumed that both P and M' have a *variable magnitude* in order to obtain the changes $\partial M / \partial P$ or $\partial M / \partial M'$.

Internal Moments M

- Establish appropriate x coordinates that are valid within regions of the beam or frame where there is no discontinuity of force, distributed load, or couple moment.
- Calculate the internal moment M as a function of P or M' and each x coordinate. Also, compute the partial derivative $\partial M / \partial P$ or $\partial M / \partial M'$ for each coordinate x .
- After M and $\partial M / \partial P$ or $\partial M / \partial M'$ have been determined, assign P or M' its numerical value if it has replaced a real force or couple moment. Otherwise, set P or M' equal to zero.

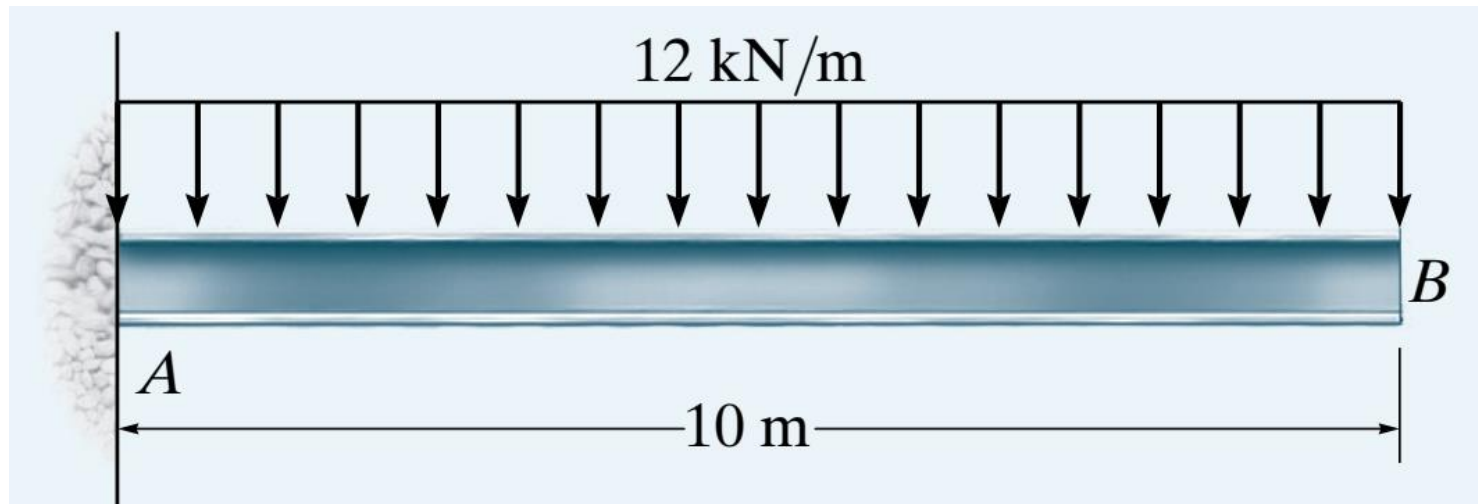
Castigliano's Theorem

- Apply Eq. 9-28 or 9-29 to determine the desired displacement Δ or slope θ . It is important to retain the algebraic signs for corresponding values of M and $\partial M / \partial P$ or $\partial M / \partial M'$.
- If the resultant sum of all the definite integrals is positive, Δ or θ is in the same direction as \mathbf{P} or \mathbf{M}' .



Example 3

- Determine the displacement of point B of the beam shown in the figure. Take $E = 200\text{GPa}$, $I = 500(10^6)\text{mm}^4$.



Solution 3

- A vertical force P is placed on the beam at B as shown in the figure.

Internal Moments M . A single x coordinate is needed for the solution, since there are no discontinuities of loading between A and B . Using the method of sections,

$$\zeta + \Sigma M = 0; \quad -M - (12x)\left(\frac{x}{2}\right) - Px = 0$$

$$M = -6x^2 - Px \quad \frac{\partial M}{\partial P} = -x$$

Setting $P = 0$, its actual value, yields

$$M = -6x^2 \quad \frac{\partial M}{\partial P} = -x$$

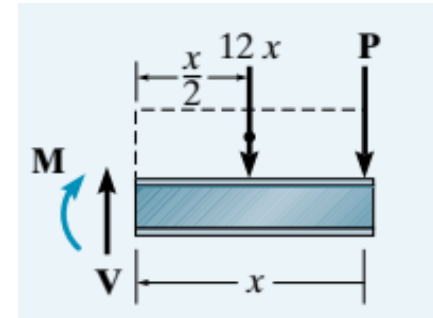
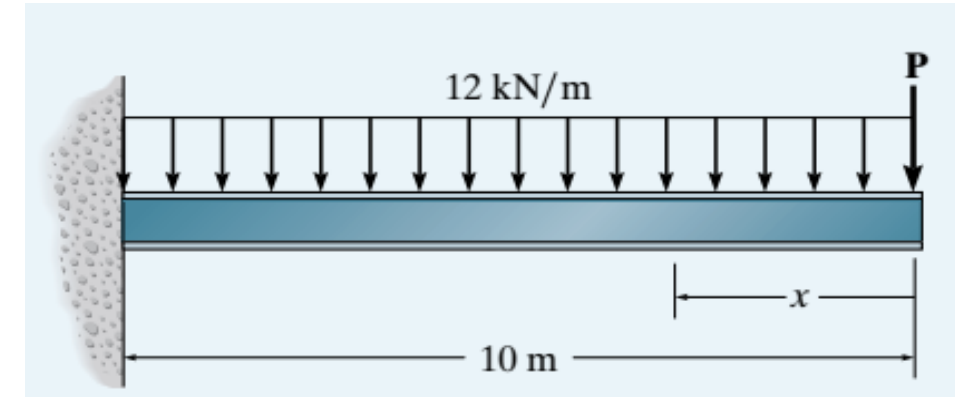
Castigliano's Theorem. Applying Eq. 9-28, we have

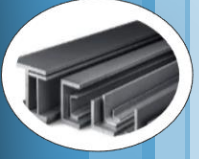
$$\Delta_B = \int_0^L M \left(\frac{\partial M}{\partial P} \right) \frac{dx}{EI} = \int_0^{10} \frac{(-6x^2)(-x)}{EI} dx = \frac{15(10^3) \text{ kN} \cdot \text{m}^3}{EI}$$

or

$$\begin{aligned} \Delta_B &= \frac{15(10^3) \text{ kN} \cdot \text{m}^3}{200(10^6) \text{ kN/m}^2 [500(10^6) \text{ mm}^4] (10^{-12} \text{ m}^4/\text{mm}^4)} \\ &= 0.150 \text{ m} = 150 \text{ mm} \end{aligned}$$

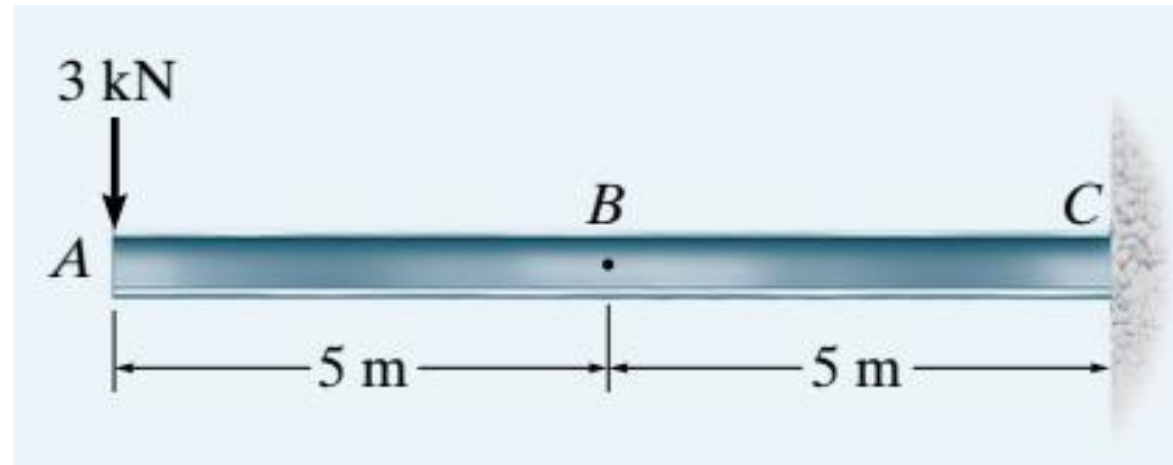
Ans.





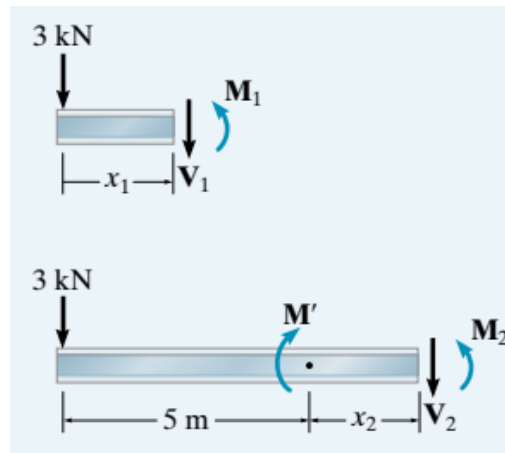
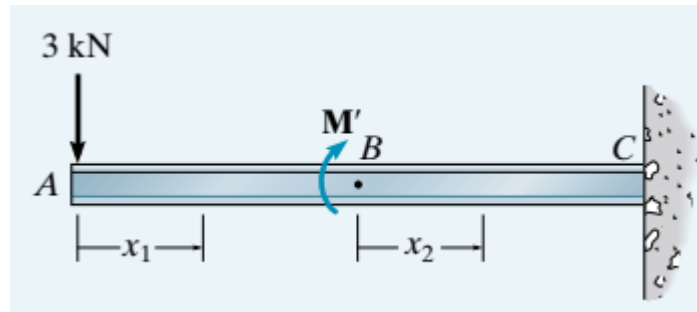
Example 4

- Determine the slope at point B of the beam shown in the figure. Take $E = 200\text{GPa}$, $I = 60(10^6)\text{mm}^4$.



Solution 4

- Since the slope at point B is to be determined, an external couple M' is placed on the beam at this point. Two coordinates, x_1 and x_2 , must be used to determine the internal moments within the beam since there is a discontinuity, M' , at B.



$$\zeta + \Sigma M = 0; \quad M_1 + 3x_1 = 0$$

$$M_1 = -3x_1$$

$$\frac{\partial M_1}{\partial M'} = 0$$

For x_2 :

$$\zeta + \Sigma M = 0; \quad M_2 - M' + 3(5 + x_2) = 0$$

$$M_2 = M' - 3(5 + x_2)$$

$$\frac{\partial M_2}{\partial M'} = 1$$

Castigliano's Theorem. Setting $M' = 0$, its actual value, and applying Eq. 9-29, we have

$$\begin{aligned} \theta_B &= \int_0^L M \left(\frac{\partial M}{\partial M'} \right) \frac{dx}{EI} \\ &= \int_0^5 \frac{(-3x_1)(0) dx_1}{EI} + \int_0^5 \frac{-3(5 + x_2)(1) dx_2}{EI} = -\frac{112.5 \text{ kN} \cdot \text{m}^2}{EI} \end{aligned}$$

or

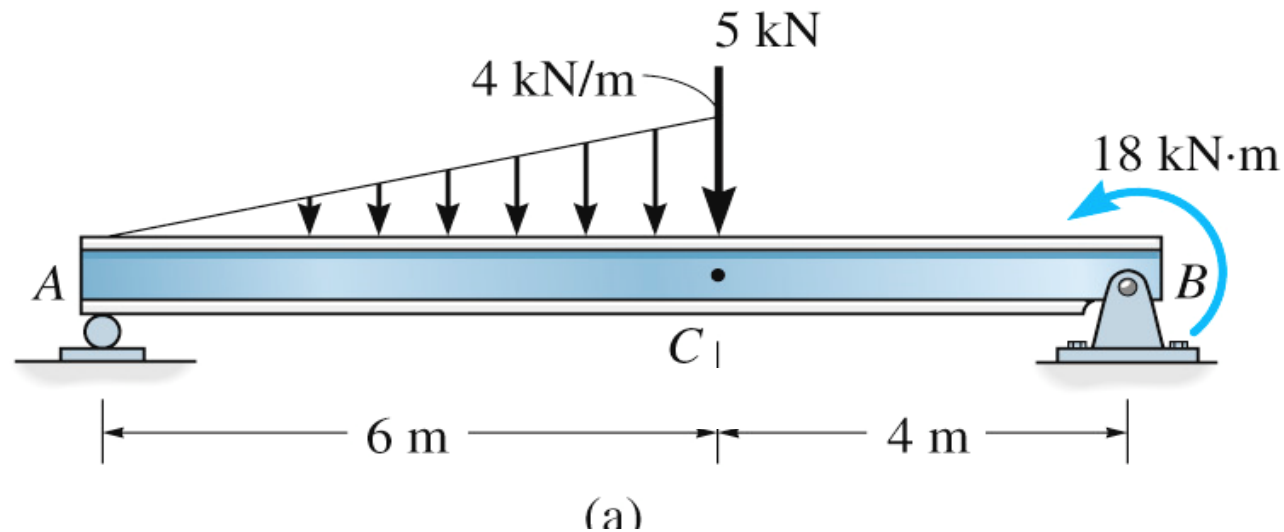
$$\begin{aligned} \theta_B &= \frac{-112.5 \text{ kN} \cdot \text{m}^2}{200(10^6) \text{ kN/m}^2 [60(10^6) \text{ mm}^4] (10^{-12} \text{ m}^4/\text{mm}^4)} \\ &= -0.00938 \text{ rad} \end{aligned}$$

Ans.

The negative sign indicates that θ_B is opposite to the direction of the couple moment M' . Note the similarity between this solution and that

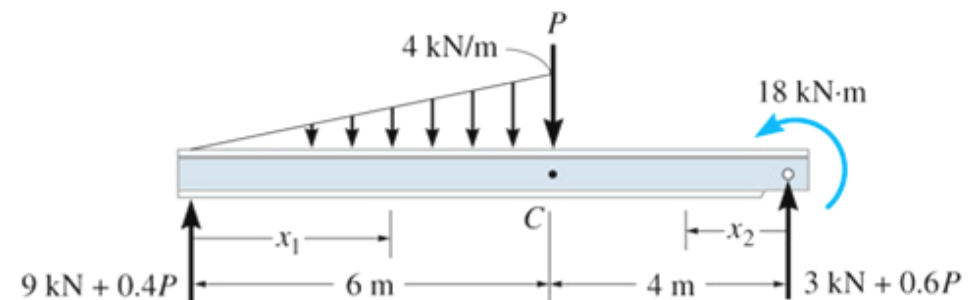
Example 5

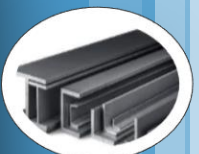
Determine the vertical displacement of point C of the steel beam shown in Fig. 14–44a. Take $E_{st} = 200 \text{ GPa}$, $I = 125(10^{-6}) \text{ m}^4$.



SOLUTION

External Force P . A vertical force P is applied at point C , Fig. 14–44b. Later this force will be set equal to the fixed value of 5 kN.





Solution 5



Internal Moments M . In this case two x coordinates are needed for the integration since the load is discontinuous at C . Using the method of sections, Fig. 14–44c, the internal moments and partial derivatives are determined as follows:

For x_1 ,

$$+\Sigma M_{NA} = 0; \quad M_1 + \frac{1}{3} x_1^2 \left(\frac{x_1}{3} \right) - (9 + 0.4P)x_1 = 0$$

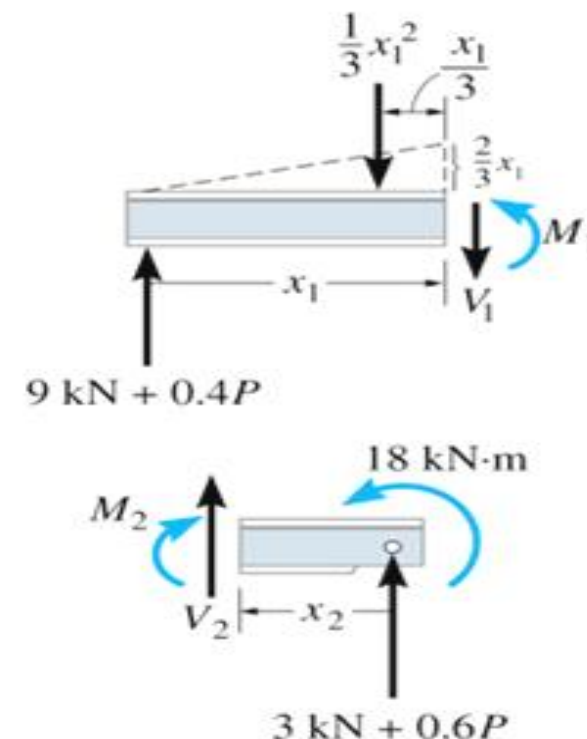
$$M_1 = (9 + 0.4P)x_1 - \frac{1}{9} x_1^3$$

$$\frac{\partial M_1}{\partial P} = 0.4x_1$$

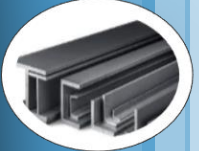
For x_2 ,

$$\downarrow + \Sigma M_{NA} = 0; \quad -M_2 + 18 + (3 + 0.6P)x_2 = 0$$

$$M_2 = 18 + (3 + 0.6P)x_2$$



(c)



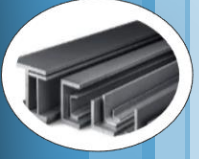
Solution 5

$$\frac{\partial M_2}{\partial P} = 0.6x_2$$

Castigliano's Second Theorem. Setting $P = 5$ kN and applying Eq. 14–49, we have

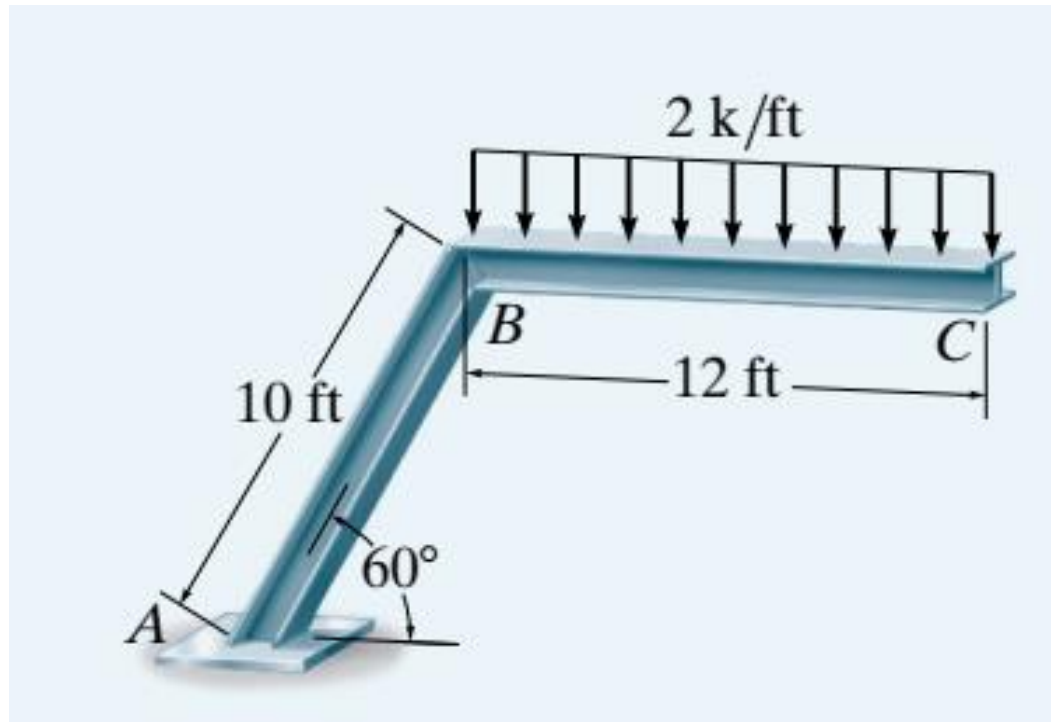
$$\begin{aligned}\Delta_{C_v} &= \int_0^L M \left(\frac{\partial M}{\partial P} \right) \frac{dx}{EI} \\ &= \int_0^6 \frac{(11x_1 - \frac{1}{9}x_1^3)(0.4x_1) dx_1}{EI} + \int_0^4 \frac{(18 + 6x_2)(0.6x_2) dx_2}{EI} \\ &= \frac{410.9 \text{ kN} \cdot \text{m}^3}{[200(10^6) \text{ kN/m}^2] 125(10^{-6}) \text{ m}^4} \\ &= 0.0164 \text{ m} = 16.4 \text{ mm}\end{aligned}$$

Ans.



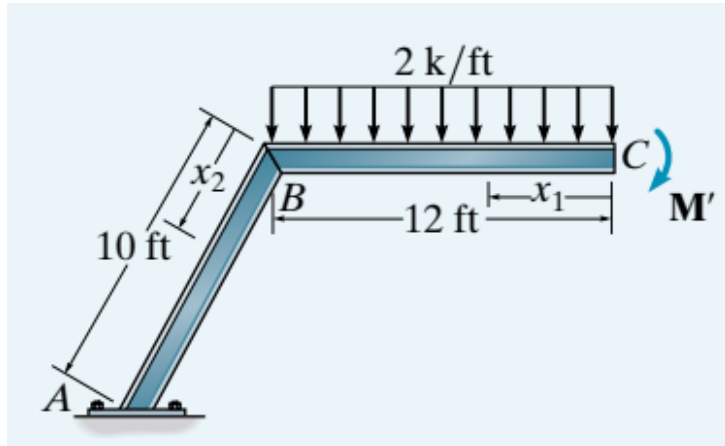
Example 6

- Determine the slope at point C of the two-member frame shown in the Figure below. The support at A is fixed. Take $E = 29000 \text{ ksi}$, $I = 600 \text{ in}^4$.



Solution 6

- A variable moment M' is applied to the frame at point C, since the slope at this point is to be determined. Due to the discontinuity of internal loading at B, two coordinates, x_1 and x_2 , are chosen



For x_1 :

$$\zeta + \Sigma M = 0; \quad -M_1 - 2x_1\left(\frac{x_1}{2}\right) - M' = 0$$

$$M_1 = -(x_1^2 + M')$$

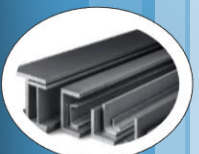
$$\frac{\partial M_1}{\partial M'} = -1$$

For x_2 :

$$\zeta + \Sigma M = 0; \quad -M_2 - 24(x_2 \cos 60^\circ + 6) - M' = 0$$

$$M_2 = -24(x_2 \cos 60^\circ + 6) - M'$$

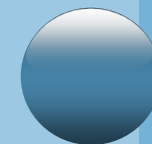
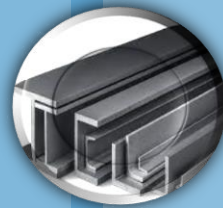
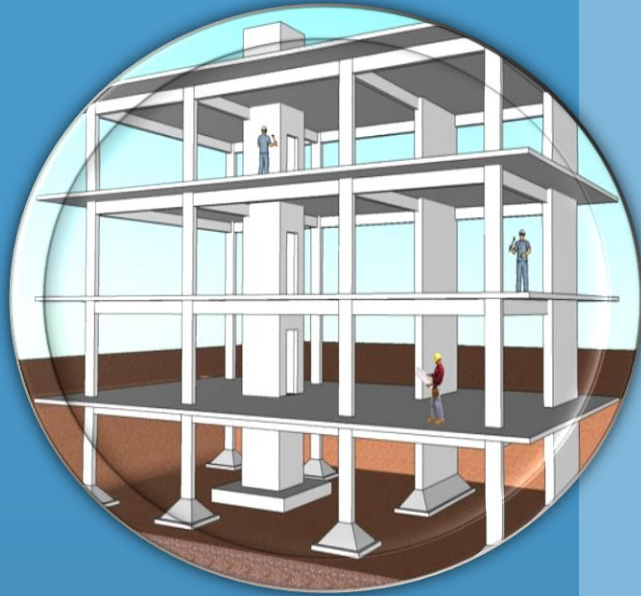
$$\frac{\partial M_2}{\partial M'} = -1$$



Solution 6

Castigliano's Theorem. Setting $M' = 0$ and applying Eq. 9-29 yields

$$\begin{aligned}\theta_C &= \int_0^L M \left(\frac{\partial M}{\partial M'} \right) \frac{dx}{EI} \\ &= \int_0^{12} \frac{(-x_1^2)(-1) dx_1}{EI} + \int_0^{10} \frac{-24(x_2 \cos 60^\circ + 6)(-1) dx_2}{EI} \\ &= \frac{576 \text{ k} \cdot \text{ft}^2}{EI} + \frac{2040 \text{ k} \cdot \text{ft}^2}{EI} = \frac{2616 \text{ k} \cdot \text{ft}^2}{EI} \\ \theta_C &= \frac{2616 \text{ k} \cdot \text{ft}^2 (144 \text{ in}^2/\text{ft}^2)}{29(10^3) \text{ k/in}^2 (600 \text{ in}^4)} = 0.0216 \text{ rad} \quad \text{Ans.}\end{aligned}$$



Thank You!